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SONIC-BOOM EXPOSURES DURING OKLAHOMA CITY COMMUNITY RESPONSE STUDIES
FOR THE PERIOD FEBRUARY THROUGH MAY 1964

By David A. Hilton, Vera Huckel, Roy Steiner,
and Domenic J. Maglieri

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LANGLEY RESEARCH CENTER
NATIONAL AERONAUTICS AND SPACE ADMINISTRATION

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INTRODUCTION

The effects of sonic booms are an important consideration in the over-land operation of supersonic aircraft. Of particular significance in the operation of proposed supersonic transports is the reaction of communities to sonic-boom exposures from repeated flights. Only a limited amount of information relative to this repeated exposure problem is available. This has led to the Oklahoma City experiments sponsored by the Federal Aviation Agency and participated in by other agencies and organizations, the NASA being responsible for the measurement of sonic boom exposures in the test area. The material of this paper is thus primarily concerned with these latter measurements. In addition to describing the sonic-boom exposure of the community, the data illustrate some of the effects of the atmosphere during sonic-boom propagation.

In previous experiments, some variations of wave shape and overpressure values were found to exist and were ascribed to atmospheric effects (see ref. 1). These effects were noted to be related to conditions of the atmosphere near the earth's surface. Such results were obtained during a rather limited series of studies both in terms of number of flights and time duration of the program. The Oklahoma City experiments have provided the opportunity to evaluate possible effects on the sonic-boom signatures of the atmosphere and weather for an extended period of time and for a relatively large number of flights.

The purpose of this paper is to document the sonic-boom pressure exposures during the above experiments and, in particular, at three measuring stations for about 800 flights in the time period February 3, 1964 to June 1, 1964. Data are tabulated for each flight so that they may be correlated with information generated by other organizations participating in this program. Included are analyses of some specific sets of data such as categorizations of waveforms and statistical breakdowns of overpressures and positive impulses.

APPARATUS AND METHODS

Test Conditions

Test flights for which data are presented were made in the Greater Oklahoma City area along the track indicated in figure 1. This general area has an elevation of about 1,700 feet above sea level and includes a population of about 750,000 people in its urban, suburban, and rural regions. Several flights per day were made starting in February 1964. The data of this paper are from those flights accomplished up to June 1, 1964. The program is scheduled to continue through the month of July, and hence the additional data results will be reported subsequently.

Test Airplanes

Photographs of the airplanes of the types used in these tests are shown in figure 2. Airplane A has an overall length of 54.5 feet and a gross weight varying from 14,000 to 19,000 pounds. Airplane B has an overall length of 57.5 feet and a gross weight varying from 34,000 to 45,000 pounds. Airplane C has an overall length of 96.8 feet and a gross weight varying from 100,000 to 116,000 pounds. Aircraft of these types have been used in other sonic-boom flight test programs and details such as area distributions, fineness ratios, and shape factors are given in references 1 and 2. The airplanes were maintained and operated by U. S. Air Force personnel.

Aircraft Operations and Positioning

The aircraft were operated in the altitude range 21,000 to 50,000 feet and the Mach number range 1.4 to 2.0. The airplanes in all cases were positioned over the test area and along the prescribed ground track (see fig. 1) by means of ground-control procedures with the aid of radar tracking. The ground controller was located in Fort Worth, Texas, and the radar antenna was located within the Oklahoma City area (see fig. 1). The majority of the flights were made on a heading of 049° magnetic. On February 19 and 29 the flights were made on a heading of 229° magnetic; on April 28 the heading for flights 1 through 4 was 310° magnetic, and flights 5 through 8 were on 130° magnetic; on April 29 flights 1 through 4 were made on a heading of 170° magnetic and flights 5 through 8 on 350° magnetic. Flights on March 7 were conducted on the 049° magnetic heading, but the airplane was displaced 8 miles to the north of the original track. Radar plotting-board overlays were obtained for all flights, and the data were used to provide information on aircraft plan position and ground velocity. Altitude was obtained from a GCI station located in Oklahoma City. All altitude values listed in the data tables are with reference to mean sea level.

Each aircraft was directed on the flight track such that the desired Mach number and altitude conditions were reached when the aircraft was in the vicinity of Minco and were maintained to the general vicinity of Arcadia. When the above procedures were used, the sonic booms observed at the measuring stations indicated in figure 1 were associated with steady-level flight conditions of the aircraft. In some cases the acceleration portion was extended beyond the point shown in figure 1 to permit two passes to be made during one flight. For some of these latter flights, acceleration effects (see ref. 3) were noted to exist in the Oklahoma City test area.

Atmospheric Soundings

Rawinsonde observations from the U. S. Air Force weather facility located at Will Rogers Field (see fig. 1) were taken within 1 hour of the times of all of the supersonic flights. Measured values of temperature and pressure, along with the calculated speed-of-sound and humidity values and wind velocity and direction values, were provided up to at least the airplane test altitude.

In addition to the 4 Rawinsonde observations which were obtained during each day, surface measurements of temperatures, winds, etc. were obtained along with information relayed by the pilots during their ascent to altitude and during the actual supersonic run. The type of information obtained from the pilots included indications of turbulence, cloud cover, and precipitation.

Pressure Instrumentation

The main components of the measurement systems used for sonic-boom pressures are the same as for reference 1. Each channel of the system as used in the experiments consisted of a specially-modified microphone, tuning unit, DC amplifier, and oscillograph recorder. The usable frequency range was from 0.1 to 5,000 cps, and this applies to all of the data presented herein. The microphones have a dynamic range from about 70 to about 150 db. They were field-calibrated statically before each test by means of a pressure bellows and a sensitive manometer. Prior to field installation, frequency response curves were obtained for all microphones.

Sonic boom pressure measurements were made both inside and outside all 3 test buildings. Each outside microphone was shock mounted at ground level in the surface of a plywood reflecting board, as shown in figure 9 of reference 1. Wind screens designed so as not to affect the pressure measurements were used at all times. When making measurements during precipitation, a thin plastic cover was draped loosely over the wind screens.

For the inside measurements, each microphone was shock mounted at approximately 5 feet from the floor level near the center of the room. The above setups were used to make inside and outside measurements at each of the 3 measuring stations noted in figure 1.

In order to obtain information on the scale and correlation of ground overpressure fluctuations, a special multiple array of microphones was used for simultaneous measurements at selected locations. Simultaneous recordings from each of 5 microphones were made for several flights for microphone separation distances from 50 to 200 feet in straight lines parallel to and perpendicular to the flight track of the aircraft. These data were taken in open areas at locations near the ground track and also at lateral distances of about 8 miles to either side of it.

RESULTS AND DISCUSSION

Wave Shapes

The type of experimental data obtained in the measurements of the present studies is illustrated in figure 3, which shows sample outside and inside sonic-boom pressure signatures. The outside pressure signature is of the N-wave type, whereas the inside pressure signature has the general appearance of a damped sine wave. The peak overpressure values in either case are defined as the maximum positive deviation from local atmospheric pressure, as indicated in the figure.

From a study of the data obtained, it was found that the outside pressure traces varied markedly in character such that it was useful to categorize them as indicated in figure 4. The characteristic wave shapes are presented on the left-hand side of the figure, with word descriptions on the right-hand side. In cases where wave shapes did not fall naturally into one of the categories illustrated, a two-letter designation was assigned. For instance, a type "NP" was judged to be intermediate between type "N" and type "P". Also shown on the figure are definitions of such quantities as positive impulse I_0 and the duration of the positive phase of the wave Δt_0 , which are listed in the main data tables along with peak overpressure and wave shape categories.

Tabulations of Data

The measured data as determined from time-history records such as those of figures 3 and 4 are listed in tables I through XIV. The data in each table are listed chronologically for each aircraft and altitude combination. In addition to the sonic-boom signature data for the 3 measurement stations, some associated weather and aircraft operating condition information is included. Where there are no entries in the table, either the data do not exist or could not be properly interpreted. Symbols, definitions, and units applicable to the information of tables I through XIV are included in table XV.

For convenience of the reader, table XVI has been prepared to include the number of data records at each measuring station for various flight conditions, along with the number of the appropriate table (see I through XIV) in which the

data are included. It is obvious from an inspection of table XVI that a much larger number of flights was conducted for some test conditions than for others, and thus these results may be of greater statistical significance.

Variations for a Series of Flights

Some of the data of tables I through XIV, for which a large number of data points are available, have been studied in detail to determine the manner in which the peak overpressure and impulse values vary. The results of these studies are included in figures 5 through 7. In these figures the data have been plotted as relative cumulative frequency distributions and thus, on the ordinate scales, give the probability of equaling or exceeding the given values of the abscissae.

The data of figure 5 illustrate the variation of the peak overpressures for altitudes of 28,000, 30,000, and 32,000 feet for airplane A at a Mach number of 1.5 for measuring stations 1, 3, and 4. The data have been plotted on semi-log paper to emphasize the variations or differences between the higher values of the distributions. Curves have been faired through the data points as an aid in interpreting the data. As an example, in figure 5(a) for station 1 it can be seen that for the 28,000-foot altitude condition, there is a probability of equaling or exceeding an overpressure value of 1.6 lbs/sq ft approximately 9% of the time. It can be seen that as altitude increases, the probability of exceeding a certain value of overpressure decreases.

It is believed that if the aircraft speed and altitude were held absolutely constant and there were no effects of the atmosphere, the overpressure values would be equal for all flights. It can be seen that the overpressure values from one flight to another are not constant, but rather vary in amplitude over a considerable range. These variations may be due to such factors as small variations in aircraft flight conditions, small variations due to measuring technique and instrument accuracies, and variations due to the weather. For the data illustrated, the weather effects are judged to be dominant.

Similar data are presented in figures 5(b) and 5(c) for measuring stations 3 and 4, respectively. Although the probability values are somewhat different than those of figure 5(a), the same general trends of the data are evident.

In figure 6(a) the data for the 32,000-foot condition of figure 5 are plotted for comparison of the measurements at the 3 measuring stations. It can be noted that the pressure exposures are very similar at stations 1 and 3 and are generally less severe at station 4. This was the general pattern of the data. During the experiments at 28,000 feet, however, as may be noted in figure 6(b), the faired curves for the data of stations 3 and 4 have a different shape and higher overpressures were experienced than at station 1. These differences in shape were noted to be associated with the data at the lateral stations for which the ray paths were longer for a given flight condition. It is not known whether the above changes in shape are due to sampling variations, a longer ray path in the presence of turbulence, a shifting of the exposure

pattern because of crosswinds (see ref. 4), or some combination of these phenomena.

In figures 5 and 6 the relative cumulative frequency distributions have been plotted on semi-log paper with curves faired through the higher values of overpressure. This manner of plotting is not intended to imply the type of distribution which would best describe the data. Although a log-normal distribution may be suggested from a theoretical consideration, no one type of distribution has given a satisfactory fit for these data over the entire range of the data.

The positive impulse functions have been determined for the experiments of figure 5 and are presented in figure 7. Semi-log plots are presented, and the data are coded in the same way as for figure 5. The variations are noted to be similar in nature to those of the overpressures illustrated in figure 5. The variation from the mean value, however, is markedly less than for the overpressures.

The data of table XVII are included as a brief summary of the overpressure and positive impulse results of the above studies for the groups of data of tables I through XIV having the highest number of data points. Included in the table are the median values (50% probability) and the values at 1% probability for each of the 3 measuring stations. Also included in the table for comparison are nominal values calculated by the method of reference 5 for conditions of a standard atmosphere with zero wind. One of the most obvious results which is illustrated by the data of the table is that the median values are generally lower than the calculated nominal values. This trend may be expected based on energy conservation considerations (see ref. 6).

Variations for a Given Flight

The data presented in tables I through XIV and in figures 5 through 7 indicate the type of variations of the pressure exposures at discrete measuring points over a period of time during which atmospheric changes occurred. In order to provide some information relative to the variations occurring in specific areas on the ground as a result of a single flight, experiments were performed with a special microphone array in which the individual microphones were accurately spaced and oriented relative to the flight track. Sample data obtained in this manner are presented in figures 8 and 9.

The data of figure 8 represent an overall calibration of the individual microphones in the array. They were placed within a few inches of each other for one of the flights in order to check for repeatability and to determine the amount of variation inherent in the field use of these instruments. Tracings were made of the pressure-time history records, and these are presented in the figure. It is obvious that the wave shapes are nearly identical, and this would be expected because the systems are closely matched in frequency response and are closely grouped to minimize atmospheric effects. As illustrated in the figure, the variation in the results from the average value which may be ascribed to instrument differences and calibration and reading errors is noted

6.

to be less than about $\pm 7\%$.

For this experiment the sensitive diaphragm element of the microphone was located about 6 inches above and parallel to the reflecting surface, and this thus accounts for the small steps in the steeply rising portions of the waves at both the initial and final compressions. The same microphone positioning scheme was used to obtain the data of figure 9.

In figure 9 are presented tracings of the measured waveforms from the above accurately-calibrated and oriented array of matched microphones. These data illustrate the variations of waveforms obtained for given flights for which the aircraft operating conditions are essentially constant. The waveforms are presented in the proper time sequence and are directly comparable in amplitude. All data of the figure were recorded for microphone separation distances of 200 feet. Data are presented for flights at times 2 hours apart on the same day. It can be seen that a wide variation in wave shape occurred even over a distance on the ground of a few hundred feet, and that the variations were different for the 2 flights. The widest variation occurred for the data of figure 9(a), where a definite progression was noted from a highly peaked wave of relatively large overpressure at the first measuring point to a rounded-off wave of relatively low overpressure. The data of figure 9(b) also suggest a definite progression of events. A study of a series of recordings such as these and others of a similar nature taken during the experiments suggests a rising and falling of the peak overpressure values along with corresponding wave shape changes as a function of distance along the ground. The peak overpressure value rises and falls as a function of distance in much the same manner as the surface level of the ocean in the presence of waves. Although not shown in the figure, significant differences in wave shape were measured at separation distances as small as 50 feet. Such variations as these, which have also been observed on other occasions (see ref. 1), are believed to result from temperature and velocity anomalies in the atmosphere, particularly the lower layers. The fact that the measured median values of table XVII are generally lower than the calculated values for a standard atmosphere is believed to result directly from the scattering effects of the atmosphere.

Lateral-Spread Patterns

In order to summarize the results pertaining to the lateral-spread patterns in the test area, the comparable pressure data are plotted in figure 10 as a function of distance from the ground track of the aircraft. Data are included for 8 flights during a particular day and include measurements made at 3 permanent measurement stations and with the use of a mobile recording station at an 8-mile distance on the opposite side of the track. For each of the permanent recording stations, 1 data point was obtained for each flight, whereas 5 data points were recorded for each flight at the mobile recording station. There is noted to be some scatter in the overpressure values at all measuring stations. The most scatter and the highest overpressures occur at station 3 for this particular day's operations. From an inspection of similar data for other days of operation, it was noted that the largest scatter and highest overpressures do not always occur at station 3, but also might occur at any of

the other stations. Also shown on the figure is a calculated curve of nominal overpressure values for these flight conditions, along with the calculated cut-off points for atmospheric refraction assuming a zero wind condition (see ref. 7). For the data shown in the figure, there was a prevailing wind generally from left to right (northwest to southeast). Such a wind occurred on the majority of the days of operation. There is a possibility of a shifting of the whole pressure pattern, generally to the right, for such wind conditions. Such a shift of the pressure pattern is judged to have occurred on some occasions when waveforms of type c (see fig. 4) were measured at the upwind measuring station. Such waveforms are consistently measured near the edge of the pressure pattern. Another result which suggests some shifting of the pressure pattern is the fact that in many cases, as for instance those of figure 10, measured overpressures at station 3 were as high as or higher than those at station 1.

Correlation Between Inside and Outside Measurements

The measured data have been analyzed for the purpose of establishing some correlation, if possible, between the inside measurements and the outside measurements. There is reason to believe that the inside microphone may give an indication of the overall dynamic response of the building since it integrates all of the pressure fluctuations in its vicinity due to motions of the building components. Such a measurement might, therefore, be significant with regard to judgements of acceptability by indoor observers. One of the findings of the above studies is illustrated in figure 11. In the upper part of the figure are shown 2 markedly different waveforms as measured for airplane A at the outside microphone measuring location of station 1. Even though the overpressure values and the associated wave shapes differ, the wavelengths are nearly the same. The bottom traces are the corresponding pressure-time histories measured at the inside microphone location of the test house. The most obvious result is that the inside pressure traces are very nearly identical despite the marked differences in the outside pressure traces.

The results of figure 11, of course, apply to a particular aircraft. Different results are obtained, as illustrated in figure 12, for different aircraft. In the top part of the figure are the outside pressure traces for aircraft A and C, and in the lower part of the figure are the corresponding inside pressure traces. Although the outside pressure traces differ in some detail, the major difference is in the wavelength. The inside pressure traces are seen to differ markedly in character, the trace with the fluctuations of lower frequency being associated with the outside wave of longer duration or wavelength.

The above results suggest that the peak pressure alone is not the dominant factor in building response, but that a combination of peak pressure and time duration (impulse) may be important. Figure 13 contains a presentation of the comparable inside and outside measurements to illustrate a possible correlation of these data. Inside peak overpressures are plotted as a function of positive impulse values as determined from outside pressure measurements and as listed in tables I through XIV. The large number of data points for aircraft A are represented by the hatched area, whereas the relatively few data for aircraft B

are shown as circles. The inside pressure values are noted to increase generally as the outside impulse values increase, and thus are higher for the larger aircraft.

CONCLUDING REMARKS

The material of this paper includes interim tabulations and analyses of the sonic-boom pressure data measured in the Oklahoma City community response experiments. The results were characterized by variations in both the peak overpressures and the impulse functions of the sonic-boom signatures due to the effects of the atmosphere. The median values of the measurements are generally lower than those predicted based on a standard atmosphere. It has not been determined at this time what type of statistical distribution describes these phenomena.

Langley Research Center,
National Aeronautics and Space Administration,
Langley Station, Hampton, Va., July 1, 1964.

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Table 1.- Summary Of Sonic Boom Data For Various Flights Of Airplane A For An
Altitude Range Of 36,000 To 41,000 Feet

OPERATING CONDITIONS				WEATHER				SONIC BOOM PRESSURE SIGNATURE DATA														
Date	Flight No.	Time	Mach No.	Surface Temp.	Surface Winds	Cloud Cover	Precipitation	Station 1					Station 3					Station 4				
								ΔP_0	ΔP_1	ΔI_0 Pos.	I_0 Pos.	Wave Shape	ΔP_0	ΔP_1	ΔI_0 Pos.	I_0 Pos.	Wave Shape	ΔP_0	ΔP_1	ΔI_0 Pos.	I_0 Pos.	Wave Shape
41,000 FT.																						
4-1-64	1/54	706	2.0	51°	200/5	0	None	1.07	-	0.045	0.047	NR	0.91	-	0.045	0.048	NR	1.0	-	0.045	0.048	NR
"	2/54	900	2.0	65°	040/5	"	"	.77	-	.048	.040	NR	1.04	-	.040	.043	NR	1.15	-	.042	.045	NR
"	3/54	900	2.0	"	"	"	"	.65	-	.046	.047	R	1.17	-	.036	.045	NR	1.17	-	.043	.044	NR
38,000 FT.																						
4-1-64	3/11	1256	1.5	33°	210/10	0	None	1.00	0.36	0.055	0.055	NR	0.82	0.30	0.055	0.053	NR	0.83	0.48	0.046	0.047	I
"	4/11	1520	1.5	38°	320/15	"	"	.70	.40	.051	.051	NR	.42	.17	.058	.051	R	.51	.42	.052	.042	NR
"	5/11	1625	1.5	37°	320/10	"	"	.72	.41	.052	.053	NR	.60	.29	.050	.048	N	.66	.48	.046	.045	NR
4-1-64	1/10	827	1.5	38°	250/10	"	"	.79	.35	.051	.046	NR	.67	.42	.048	.045	NR	-	-	-	-	NR
"	2/10	1021	1.5	45°	200/10	"	"	.21	.41	.047	.046	NR	.63	.37	.050	.046	NR	.64	.46	.043	.042	NR
"	3/10	1255	1.5	54°	250/1500	"	"	1.16	.45	.041	.045	N	.96	.21	.050	.0430	NR	.71	.30	.061	.047	NR
"	4/10	1521	1.5	56°	240/15	"	"	.84	.40	.046	.045	NR	.75	.27	.048	.0490	NR	.79	.48	.052	.042	NR
"	5/10	1758	1.5	"	"	"	"	.88	.41	.045	.044	NR	.75	.31	.047	.044	NR	.96	.49	.048	.045	NR
4-1-64	1/10	700	1.5	"	"	"	"	.88	.39	.046	.044	NR	.54	.30	.053	.0403	NR	.96	.30	.050	.046	NR
"	2/10	758	1.5	31°	330/15	"	"	-	-	-	-	NR	.67	.34	.053	.0417	NR	-	.45	-	-	NR
"	3/10	758	1.5	"	"	"	"	.40	.36	.051	.0433	NR	.68	.48	.052	.0417	N	.44	.43	.060	.048	R
37,000 FT.																						
4-4-64	1/1	1047	1.5	39°	080/10	⊕	None	0.77	0.54	0.056	0.0487	R	-	-	-	-	-	-	-	-	-	-
4-5-64	1/2	1256	1.5	38°	360/15	"	RW	.74	.52	.056	.0477	NR	-	-	-	-	-	.34	.42	.046	.0400	NR
"	3/4	1524	1.5	39°	340/10	"	"	.71	.51	.055	.0474	NR	.82	.31	.050	.0445	N	.47	.70	.046	.0447	NR
4-6-64	4/8	1754	1.5	39°	360/1500	"	None	.86	.46	.044	.043	NR	.83	.48	.048	.0474	N	.57	.41	.050	.0447	NR
4-7-64	1/9	827	1.5	24°	330/5	⊕	"	1.30	.49	.044	.043	R	.98	.27	.046	.0435	N	.74	.46	-	-	NR
"	2/10	1027	1.5	36°	"	"	"	.86	.31	.045	.0434	NR	1.04	.21	.047	.0423	N	.74	.47	.051	.0420	I
36,000 FT.																						
4-5-64	1/3	1256	1.5	35°	360/15	⊕	RW	0.59	0.45	0.052	0.0476	-	-	-	-	-	-	0.39	0.60	0.060	0.042	NR
4-6-64	1/5	1027	1.5	41°	350/10	⊕	None	.70	.45	.047	.0471	NR	1.06	.27	.047	.0476	N	1.01	.30	-	-	NR
"	2/6	1254	1.5	41°	"	"	"	1.17	.45	.046	.0474	NR	.87	.27	.047	.0471	N	.65	.48	.048	.0451	NR
"	3/7	1521	1.5	41°	360/10	"	"	1.03	.37	.044	.043	NR	.77	.27	.047	.0470	N	.53	.40	.045	.0471	NR
4-6-64	1/10	826	1.5	41°	240/10	⊕	"	.84	.37	.048	.043	NR	.82	.27	.047	.0471	N	.53	.40	.045	.0471	NR
"	2/10	1027	1.5	70°	200/15	⊕	"	.71	.45	.045	.047	N	.70	.26	.041	.0461	NR	.61	.41	.044	.0454	NR
"	3/10	1527	1.5	50°	215/10	"	"	.75	.45	.045	.047	N	.72	.21	.047	.0474	NR	.60	.44	.046	.0458	NR
"	4/10	1754	1.5	45°	"	"	"	.75	.45	.045	.047	N	.72	.21	.047	.0474	NR	.60	.44	.046	.0458	NR
"	5/10	1754	1.5	45°	"	"	"	.75	.45	.045	.047	N	.72	.21	.047	.0474	NR	.60	.44	.046	.0458	NR
"	6/10	1754	1.5	45°	"	"	"	.75	.45	.045	.047	N	.72	.21	.047	.0474	NR	.60	.44	.046	.0458	NR
"	7/10	1754	1.5	45°	"	"	"	.75	.45	.045	.047	N	.72	.21	.047	.0474	NR	.60	.44	.046	.0458	NR

Table II.- Summary Of Sonic Boom Data For Various Flights Of Airplane A For An
Altitude Range Of 33,000 To 35,000 Feet

OPERATING CONDITIONS				WEATHER				SONIC BOOM PRESSURE SIGNATURE DATA															
Date	Flight No.	Time	Mach No.	Surface Temp.	Surface Winds	Cloud Cover	Precipitation	Station 1					Station 3					Station 4					
								ΔP_0	ΔP_1	Δt_0 Pos.	I_0 Pos.	Wave Shape	ΔP_0	ΔP_1	Δt_0 Pos.	I_0 Pos.	Wave Shape	ΔP_0	ΔP_1	Δt_0 Pos.	I_0 Pos.	Wave Shape	
35,000 FT.																							
10-10-64	1/10	13:57	1.5	22°	240/10	☉	None	1.15	0.25	0.043	0.0219	NR	0.74	0.26	0.070	0.0171	NR	0.55	0.11	0.028	0.010	NR	NR
10-10-64	1/10	13:58	1.5	21°	240	☉	"	0.97	0.31	0.045	0.027	R	0.78	0.31	0.070	0.0207	NR	0.45	0.21	0.027	0.010	NR	NR
10-10-64	1/17	7:01	1.5	25°	160/10	☉	"	1.96	0.38	0.046	0.027	N	1.03	0.31	0.071	0.0207	NR	0.66	0.27	0.027	0.015	NR	NR
10-10-64	1/17	7:01	1.5	25°	240/10	☉	"	1.32	0.31	0.045	0.027	NR	0.78	0.31	0.070	0.0207	NR	0.94	0.21	0.027	0.017	NR	NR
10-10-64	1/17	7:01	1.5	25°	"	☉	"	1.10	0.31	0.045	0.027	NR	1.33	0.31	0.070	0.0207	NR	1.12	0.18	0.027	0.017	NR	NR
10-10-64	1/17	6:58	1.5	21°	240/10	☉	TRW	0.58	0.19	0.044	0.025	-	1.74	0.57	0.070	0.0207	NR	0.47	0.11	0.027	0.015	NR	NR
10-10-64	1/17	7:01	1.5	"	"	"	"	1.16	0.39	0.052	0.027	NR	0.74	0.35	0.070	0.0207	NR	0.47	0.11	0.027	0.015	NR	NR
35,000 FT.																							
10-10-64	1/10	13:59	1.5	40°	240/10	☉	None	0.71	0.36	0.054	0.027	R	0.74	0.37	0.070	0.0207	NR	0.55	0.10	0.027	0.015	NR	NR
10-10-64	1/11	7:00	1.5	20°	160/10	☉	"	0.78	0.35	0.045	0.027	R	1.04	0.36	0.070	0.0207	NR	0.60	0.16	0.027	0.015	NR	NR
10-10-64	1/11	7:01	1.5	"	"	"	"	1.00	0.37	0.050	0.027	NR	0.97	0.36	0.070	0.0207	NR	0.71	0.19	0.027	0.015	NR	NR
10-10-64	1/11	7:01	1.5	20°	240/10	☉	"	1.00	0.37	0.050	0.027	NR	0.97	0.36	0.070	0.0207	NR	0.71	0.19	0.027	0.015	NR	NR
10-10-64	1/11	7:00	1.5	"	"	"	"	1.06	0.33	0.041	0.027	NR	1.04	0.35	0.070	0.0207	NR	0.75	0.14	0.027	0.017	NR	NR
10-10-64	1/11	7:01	1.5	20°	180/10	☉	"	0.70	0.38	0.047	0.025	NR	0.76	0.39	0.070	0.0207	NR	0.57	0.10	0.027	0.015	NR	NR
10-10-64	1/11	7:00	1.5	"	"	"	"	0.70	0.30	0.044	0.027	NR	0.73	0.35	0.070	0.0207	NR	0.57	0.10	0.027	0.015	NR	NR
35,000 FT.																							
10-10-64	1/11	6:59	1.5	18°	240/10	☉	"	1.05	0.47	0.043	0.024	NR	1.04	0.40	0.070	0.0207	NR	1.03	0.37	0.041	0.025	NR	NR
10-10-64	1/11	7:00	1.5	"	"	"	"	0.97	0.41	0.045	0.027	NR	1.01	0.35	0.070	0.0207	NR	0.63	0.30	0.044	0.025	NR	NR
10-10-64	1/11	7:00	1.5	28°	180/15	☉	"	0.87	0.37	0.046	0.025	NR	0.91	0.37	0.070	0.0207	NR	0.99	0.26	0.046	0.025	NR	NR
10-10-64	1/11	7:00	1.5	"	"	"	"	0.85	0.35	0.046	0.025	NR	0.73	0.35	0.070	0.0207	NR	0.70	0.24	0.046	0.025	NR	NR
10-10-64	1/11	7:00	1.5	29°	"	☉	"	0.74	0.34	0.046	0.025	NR	0.88	0.37	0.070	0.0207	NR	1.00	0.37	0.050	0.025	NR	NR
10-10-64	1/11	7:00	1.5	24°	240/10	"	TRW	0.61	0.30	0.041	0.025	NR	1.03	0.44	0.070	0.0207	NR	0.70	0.13	0.028	0.024	NR	NR
10-10-64	1/17	13:20	1.5	"	"	"	"	0.67	0.31	0.047	0.025	NR	1.01	0.35	0.070	0.0207	NR	0.73	0.23	0.050	0.025	NR	NR
35,000 FT.																							
10-10-64	1/17	7:00	1.5	51°	170/10	☉	FWF	0.81	0.31	0.051	0.024	R	0.70	0.35	0.070	0.0207	NR	1.17	0.35	0.041	0.024	NR	NR
10-10-64	1/17	7:00	1.5	"	"	"	"	1.35	0.34	0.044	0.025	NR	1.33	0.41	0.070	0.0207	NR	0.74	0.26	0.044	0.025	NR	NR
10-10-64	1/17	7:00	1.5	55°	"	"	FWTF	1.11	0.37	0.049	0.025	NR	0.78	0.37	0.070	0.0207	NR	0.78	0.26	0.044	0.025	NR	NR
10-10-64	1/17	7:00	1.5	"	"	"	"	1.11	0.35	0.048	0.025	NR	1.03	0.34	0.070	0.0207	NR	1.16	0.26	0.044	0.025	NR	NR
10-10-64	1/17	7:00	1.5	61°	240/10	☉	None	1.21	0.44	0.046	0.025	NR	1.03	0.34	0.070	0.0207	NR	1.16	0.26	0.044	0.025	NR	NR
10-10-64	1/17	7:00	1.5	"	"	"	"	1.21	0.44	0.046	0.025	NR	1.03	0.34	0.070	0.0207	NR	1.16	0.26	0.044	0.025	NR	NR
10-10-64	1/17	7:00	1.5	51°	240/10	☉	"	1.21	0.44	0.046	0.025	NR	1.03	0.34	0.070	0.0207	NR	1.16	0.26	0.044	0.025	NR	NR
10-10-64	1/17	7:00	1.5	51°	240/10	☉	"	1.21	0.44	0.046	0.025	NR	1.03	0.34	0.070	0.0207	NR	1.16	0.26	0.044	0.025	NR	NR
35,000 FT.																							
10-10-64	1/17	7:00	1.5	51°	240/10	☉	"	1.21	0.44	0.046	0.025	NR	1.03	0.34	0.070	0.0207	NR	1.16	0.26	0.044	0.025	NR	NR
35,000 FT.																							
10-10-64	1/17	7:00	1.5	51°	240/10	☉	"	1.21	0.44	0.046	0.025	NR	1.03	0.34	0.070	0.0207	NR	1.16	0.26	0.044	0.025	NR	NR
35,000 FT.																							
10-10-64	1/17	7:00	1.5	51°	240/10	☉	"	1.21	0.44	0.046	0.025	NR	1.03	0.34	0.070	0.0207	NR	1.16	0.26	0.044	0.025	NR	NR
35,000 FT.																							
10-10-64	1/17	7:00	1.5	51°	240/10	☉	"	1.21	0.44	0.046	0.025	NR	1.03	0.34	0.070	0.0207	NR	1.16	0.26	0.044	0.025	NR	NR
35,000 FT.																							
10-10-64	1/17	7:00	1.5	51°	240/10	☉	"	1.21	0.44	0.046	0.025	NR	1.03	0.34	0.070	0.0207	NR	1.16	0.26	0.044	0.025	NR	NR
35,000 FT.																							
10-10-64	1/17	7:00	1.5	51°	240/10	☉	"	1.21	0.44	0.046	0.025	NR	1.03	0.34	0.070	0.0207	NR	1.16	0.26	0.044	0.025	NR	NR
35,000 FT.																							
10-10-64	1/17	7:00	1.5	51°	240/10	☉	"	1.21	0.44	0.046	0.025	NR	1.03	0.34	0.070	0.0207	NR	1.16	0.26	0.044	0.025	NR	NR
35,000 FT.																							
10-10-64	1/17	7:00	1.5	51°	240/10	☉	"	1.21	0.44	0.046	0.025	NR	1.03	0.34	0.070	0.0207	NR	1.16	0.26	0.044	0.025	NR	NR
35,000 FT.																							
10-10-64	1/17	7:00	1.5	51°	240/10	☉	"	1.21	0.44	0.046	0.025	NR	1.03	0.34	0.070	0.0207	NR	1.16	0.26	0.044	0.025	NR	NR
35,000 FT.																							
10-10-64	1/17	7:00	1.5	51°	240/10	☉	"	1.21	0.44	0.046	0.025	NR	1.03	0.34	0.070	0.0207	NR	1.16	0.26	0.044	0.025	NR	NR
35,000 FT.																							
10-10-64	1/17	7:00	1.5	51°	240/10	☉	"	1.21	0.44	0.046	0.025	NR	1.03	0.34	0.070	0.0207	NR	1.16	0.26	0.044	0.025	NR	NR
35,000 FT.																							
10-10-64	1/17	7:00	1.5	51°	240/10	☉	"	1.21	0.44	0.046	0.025	NR	1.03	0.34	0.070	0.0207	NR	1.16	0.26	0.044	0.025	NR	NR
35,000 FT.																							
10-10-64	1/17	7:00	1.5	51°	240/10	☉	"	1.21	0.44	0.046	0.025	NR	1.03	0.34	0.070	0.0207	NR	1.16	0.26	0.044	0.025	NR	NR
35,000 FT.																							
10-10-64	1/17	7:00	1.5	51°	240/10	☉	"	1.21	0.44	0.046	0.025	NR	1.03	0.34	0.070	0.0207	NR	1.16	0.26	0.044	0.025	NR	NR
35,000 FT.																							
10-10-64	1/17	7:00	1.5	51°	240/10	☉	"	1.21	0.44	0.046	0.025	NR	1.03	0.34	0.070	0.0207	NR	1.16	0.26	0.044	0.025	NR	NR
35,000 FT.																							
10-10-64	1/17	7:00	1.5	51°	240/10	☉	"	1.21	0.44	0.046	0.025	NR	1.03	0.34	0.070	0.0207	NR	1.16	0.26	0.044	0.025	NR	NR
35,000 FT.																							
10-10-64	1/17	7:00	1.5	51°	240/10	☉	"	1.21	0.44	0.046	0.025	NR	1.03	0.34	0.070	0.0207	NR	1.16	0.26	0.044	0.025	NR	NR
35,000 FT.																							
10-10-64	1/17	7:00	1.5	51°	240/10	☉	"	1.21	0.44	0.046	0.025	NR	1.03	0.34	0.070	0.0207	NR	1.16	0.26	0.044	0.025	NR	NR
35,000 FT.																							
10-10-64	1/17	7:00	1.5	51°	240/10	☉	"	1.21	0.44	0.046	0.025	NR	1.03	0.34	0.070	0.0207	NR	1.16	0.26	0.044	0.025	NR	NR
35,000 FT.																							
10-10-64	1/17	7:00	1.5	51°	240/10	☉	"	1.21	0.44	0.046	0.025	NR	1.03	0.34	0.070	0.0207	NR	1.16	0.26	0.044	0.025	NR	NR
35,000 FT.																							
10-10-64	1/17	7:00	1.5	51°	240/10	☉	"	1.21	0.44	0.046	0.025	NR	1.03	0.34	0.070	0.0207	NR	1.16	0.26	0.044	0.025	NR	NR
35,000 FT.																							
10-10-64	1/17	7:00	1.5	51°	240/10	☉	"	1.21	0.44	0.046	0.025	NR	1.03	0.34	0.070	0.0207	NR	1.16	0.26	0.044	0.025	NR	NR
35,000 FT.																							
10-10-64-																							

Table III. - Summary Of Sonic Boom Data For Various Flights Of Airplane A
For An Altitude Of 32,000 Feet

OPERATING CONDITIONS				WEATHER				SONIC BOOM PRESSURE SIGNATURE DATA														
Date	Flight No.	Time	Mach No.	Surface Temp.	Surface Winds	Cloud Cover	Precipitation	Station 1					Station 3					Station 4				
								ΔP_0	ΔP_1	Δt_0 Pos	I_0 Pos	Wave Shape	ΔP_0	ΔP_1	Δt_0 Pos	I_0 Pos	Wave Shape	ΔP_0	ΔP_1	Δt_0 Pos	I_0 Pos	Wave Shape
4-1-64	3162	720	1.5	37°	25/10	①	None	1.10	.041	.047	.0434	N	1.40	.031	.044	.0477	T	.072	.027	.046	.041	N
"	4161	1200	1.5	"	"	"	"	1.24	.042	.045	.0454	NR	1.24	.031	.040	.041	C	1.03	.026	.045	.041	N
"	5160	1206	1.5	50°	350/1500	"	"	.72	.03	.053	.0410	NR	1.00	.02	.040	.0438	T	1.02	.021	.044	.040	N
"	6161	1208	1.5	"	"	"	"	1.00	.04	.056	.0410	NR	1.11	.02	.040	.0447	NP	.91	.02	.045	.040	N
"	7161	1208	1.5	50°	350/10	"	"	.91	.036	.051	.0498	NR	1.11	.02	.040	.0447	NP	.91	.02	.044	.040	N
"	8161	1208	1.5	"	"	"	"	.72	.03	.053	.0414	NR	1.02	.02	.040	.0447	NP	.91	.02	.045	.040	N
4-1-64	1161	701	1.5	58°	120/10	"	"	1.10	.047	.044	.0464	N	1.03	.02	.040	.0414	N	.61	.02	.045	.040	N
"	1263	701	1.5	"	"	"	"	-	-	-	-	-	.03	.02	.040	.0414	N	.61	.02	.045	.040	N
"	3161	720	1.5	26°	"	"	"	.97	.04	.045	.0420	NR	1.04	.02	.040	.0414	NR	.87	.02	.045	.040	N
"	4161	1200	1.5	"	"	"	"	1.12	.04	.043	.0475	N	1.02	.02	.040	.0414	NP	.87	.02	.045	.040	N
"	5161	1200	1.5	45°	"	①	"	1.19	.04	.043	.0463	N	1.15	.02	.040	.0414	N	.90	.02	.045	.040	N
"	6161	1200	1.5	"	"	"	"	.81	.03	.045	.0428	R	1.15	.02	.040	.0414	N	.65	.02	.045	.040	N
4-1-64	1161	701	1.5	30°	240/15	①	"	.85	.04	.043	.0499	R	-	-	-	-	-	.84	.02	.045	.040	N
"	2161	701	1.5	"	"	"	"	.81	.04	.045	.0471	R	-	-	-	-	-	.84	.02	.045	.040	N
"	3161	700	1.5	40°	180/150	L	"	.85	.04	.045	.0471	R	-	-	-	-	-	.84	.02	.045	.040	N
"	4161	700	1.5	"	"	"	"	1.40	.05	.041	.0476	P	-	-	-	-	-	.49	.02	.045	.040	N
4-1-64	1161	700	1.5	35°	240/10+15	①	None	.81	.035	.047	.0457	R	.66	.025	.046	.0465	R	-	-	-	-	-
"	2161	700	1.5	"	"	"	"	1.02	.035	.045	.0454	R	.87	.02	.046	.0465	R	-	-	-	-	-
"	3161	700	1.5	45°	090/4	"	"	1.12	-	.043	.0474	R	1.02	.02	.041	.0457	NP	1.12	.02	.045	.040	N
"	4161	700	1.5	"	"	"	"	1.02	-	.043	.0457	NR	.92	.02	.041	.0457	NR	1.12	.02	.045	.040	N
4-1-64	1161	701	1.5	30°	160/10	①	"	.96	-	-	-	-	1.12	.02	.041	.0457	N	.88	.02	.045	.040	N
"	2161	701	1.5	"	"	"	"	-	-	-	-	-	1.02	.02	.041	.0457	N	.88	.02	.045	.040	N
"	3161	701	1.5	36°	180/10+15	"	"	1.01	-	-	-	-	1.02	.02	.041	.0457	N	.88	.02	.045	.040	N
"	4161	701	1.5	"	"	"	"	1.27	.04	.041	.0458	NP	.70	.02	.041	.0457	N	.71	.02	.045	.040	N
"	5161	1200	1.5	50°	180/10	①	"	1.32	.04	.043	.0459	NP	-	-	-	-	-	1.27	.02	.045	.040	N
"	6161	1200	1.5	"	"	"	"	1.02	.04	.043	.0454	NR	-	-	-	-	-	1.02	.02	.045	.040	N
"	7160	1200	1.5	"	"	"	"	1.02	.04	.043	.0454	NR	.82	.02	.040	.0454	NR	.67	.02	.045	.040	N
"	7161	1201	1.5	"	"	"	"	.87	.03	.043	.0471	NR	.82	.02	.040	.0454	NR	.67	.02	.045	.040	N
4-15-64	1163	701	1.5	33°	160/10	①	"	1.01	.03	.040	.0471	NP	.82	.02	.040	.0454	NR	.67	.02	.045	.040	N
"	2164	701	1.5	"	"	"	"	1.11	.036	.047	.0471	NR	1.12	.02	.041	.0454	N	.70	.02	.045	.040	N
"	3163	701	1.5	28°	340/10+15	①	"	1.04	.037	.045	.0454	T	1.12	.02	.041	.0454	N	.70	.02	.045	.040	N
"	4163	1200	1.5	40°	230/15+15	①	"	.87	.04	.043	.0454	N	.82	.02	.040	.0454	N	.67	.02	.045	.040	N
"	5163	1200	1.5	"	"	"	"	.87	.04	.043	.0454	N	.82	.02	.040	.0454	N	.67	.02	.045	.040	N
"	6163	1200	1.5	"	"	"	"	.87	.04	.043	.0454	N	.82	.02	.040	.0454	N	.67	.02	.045	.040	N
"	7163	1200	1.5	"	"	"	"	.87	.04	.043	.0454	N	.82	.02	.040	.0454	N	.67	.02	.045	.040	N
"	8163	1200	1.5	"	"	"	"	.87	.04	.043	.0454	N	.82	.02	.040	.0454	N	.67	.02	.045	.040	N
"	9163	1200	1.5	"	"	"	"	.87	.04	.043	.0454	N	.82	.02	.040	.0454	N	.67	.02	.045	.040	N
"	10163	1200	1.5	"	"	"	"	.87	.04	.043	.0454	N	.82	.02	.040	.0454	N	.67	.02	.045	.040	N
"	11163	1200	1.5	"	"	"	"	.87	.04	.043	.0454	N	.82	.02	.040	.0454	N	.67	.02	.045	.040	N
"	12163	1200	1.5	"	"	"	"	.87	.04	.043	.0454	N	.82	.02	.040	.0454	N	.67	.02	.045	.040	N

Table III.- Continued.

OPERATING CONDITIONS				WEATHER				SONIC BOOM PRESSURE SIGNATURE DATA														
Date	Flight No.	Time	Mach No.	Surface Temp.	Surface Winds	Cloud Cover	Precipitation	Station 1					Station 3					Station 4				
								ΔP_0	ΔP_1	ΔI_0 Pos	I_0 Pos	Wave Shape	ΔP_0	ΔP_1	ΔI_0 Pos	I_0 Pos	Wave Shape	ΔP_0	ΔP_1	ΔI_0 Pos	I_0 Pos	Wave Shape
10-10-54	71	1500	1.5	25°	160/15K	⊙	None	1.27	0.51	0.046	0.074	NR	1.31	0.32	0.030	0.070	NR	1.12	0.25	0.047	0.079	NR
"	71	1505	1.5	50°	"	"	RW	1.32	0.57	0.047	0.071	NR	1.27	0.36	0.041	0.077	N	1.18	0.19	0.057	0.075	NR
"	71	1510	1.5	"	"	"	"	1.32	0.57	0.045	0.074	NR	1.31	0.32	0.041	0.077	N	1.18	0.19	0.057	0.075	NR
"	71	1515	1.5	45°	120/10	"	"	1.32	0.57	0.045	0.074	NR	1.31	0.32	0.041	0.077	NR	1.18	0.19	0.057	0.075	NR
10-10-54	71	1520	1.5	28°	220/15	⊙	None	1.27	0.40	0.045	0.074	NR	1.26	0.32	0.041	0.077	NR	1.18	0.19	0.057	0.075	NR
"	71	1525	1.5	"	"	"	"	1.27	0.40	0.045	0.074	NR	1.26	0.32	0.041	0.077	NR	1.18	0.19	0.057	0.075	NR
"	71	1530	1.5	50°	220/15	"	"	1.27	0.40	0.045	0.074	NR	1.26	0.32	0.041	0.077	NR	1.18	0.19	0.057	0.075	NR
"	71	1535	1.5	"	220/15	"	"	1.27	0.40	0.045	0.074	NR	1.26	0.32	0.041	0.077	NR	1.18	0.19	0.057	0.075	NR
"	71	1540	1.5	"	"	"	"	1.27	0.40	0.045	0.074	NR	1.26	0.32	0.041	0.077	NR	1.18	0.19	0.057	0.075	NR
"	71	1545	1.5	"	"	"	"	1.27	0.40	0.045	0.074	NR	1.26	0.32	0.041	0.077	NR	1.18	0.19	0.057	0.075	NR
"	71	1550	1.5	"	"	"	"	1.27	0.40	0.045	0.074	NR	1.26	0.32	0.041	0.077	NR	1.18	0.19	0.057	0.075	NR
"	71	1555	1.5	"	"	"	"	1.27	0.40	0.045	0.074	NR	1.26	0.32	0.041	0.077	NR	1.18	0.19	0.057	0.075	NR
"	71	1600	1.5	25°	200/15K	"	"	1.27	0.40	0.045	0.074	NR	1.26	0.32	0.041	0.077	NR	1.18	0.19	0.057	0.075	NR
"	71	1605	1.5	"	"	"	"	1.27	0.40	0.045	0.074	NR	1.26	0.32	0.041	0.077	NR	1.18	0.19	0.057	0.075	NR
"	71	1610	1.5	45°	220/10	"	"	1.27	0.40	0.045	0.074	NR	1.26	0.32	0.041	0.077	NR	1.18	0.19	0.057	0.075	NR
"	71	1615	1.5	33°	030/15	⊙	"	1.27	0.40	0.045	0.074	NR	1.26	0.32	0.041	0.077	NR	1.18	0.19	0.057	0.075	NR
"	71	1620	1.5	"	"	"	"	1.27	0.40	0.045	0.074	NR	1.26	0.32	0.041	0.077	NR	1.18	0.19	0.057	0.075	NR
"	71	1625	1.5	31°	010/10+9	⊕	S	1.01	0.37	0.050	0.076	NR	1.31	0.29	0.051	0.075	NR	1.12	0.24	0.051	0.074	NR
"	71	1630	1.5	"	"	"	"	1.17	0.37	0.049	0.076	NR	1.29	0.29	0.050	0.075	NR	1.10	0.24	0.050	0.074	NR
"	71	1635	1.5	"	"	"	"	1.27	0.40	0.045	0.074	NR	1.26	0.32	0.041	0.077	NR	1.18	0.19	0.057	0.075	NR
"	71	1640	1.5	27°	250/15K	⊕	None	1.25	0.33	0.044	0.073	NR	1.25	0.31	0.045	0.072	NR	1.17	0.22	0.051	0.073	NR
"	71	1645	1.5	"	"	"	"	1.25	0.33	0.044	0.073	NR	1.25	0.31	0.045	0.072	NR	1.17	0.22	0.051	0.073	NR
"	71	1650	1.5	70°	250/5	⊕	"	1.25	0.33	0.044	0.073	NR	1.25	0.31	0.045	0.072	NR	1.17	0.22	0.051	0.073	NR
"	71	1655	1.5	"	"	"	"	1.25	0.33	0.044	0.073	NR	1.25	0.31	0.045	0.072	NR	1.17	0.22	0.051	0.073	NR
"	71	1700	1.5	"	"	"	"	1.25	0.33	0.044	0.073	NR	1.25	0.31	0.045	0.072	NR	1.17	0.22	0.051	0.073	NR
"	71	1705	1.5	"	"	"	"	1.25	0.33	0.044	0.073	NR	1.25	0.31	0.045	0.072	NR	1.17	0.22	0.051	0.073	NR
"	71	1710	1.5	"	"	"	"	1.25	0.33	0.044	0.073	NR	1.25	0.31	0.045	0.072	NR	1.17	0.22	0.051	0.073	NR
"	71	1715	1.5	"	"	"	"	1.25	0.33	0.044	0.073	NR	1.25	0.31	0.045	0.072	NR	1.17	0.22	0.051	0.073	NR
"	71	1720	1.5	"	"	"	"	1.25	0.33	0.044	0.073	NR	1.25	0.31	0.045	0.072	NR	1.17	0.22	0.051	0.073	NR
"	71	1725	1.5	"	"	"	"	1.25	0.33	0.044	0.073	NR	1.25	0.31	0.045	0.072	NR	1.17	0.22	0.051	0.073	NR
"	71	1730	1.5	"	"	"	"	1.25	0.33	0.044	0.073	NR	1.25	0.31	0.045	0.072	NR	1.17	0.22	0.051	0.073	NR
"	71	1735	1.5	"	"	"	"	1.25	0.33	0.044	0.073	NR	1.25	0.31	0.045	0.072	NR	1.17	0.22	0.051	0.073	NR
"	71	1740	1.5	"	"	"	"	1.25	0.33	0.044	0.073	NR	1.25	0.31	0.045	0.072	NR	1.17	0.22	0.051	0.073	NR
"	71	1745	1.5	"	"	"	"	1.25	0.33	0.044	0.073	NR	1.25	0.31	0.045	0.072	NR	1.17	0.22	0.051	0.073	NR
"	71	1750	1.5	"	"	"	"	1.25	0.33	0.044	0.073	NR	1.25	0.31	0.045	0.072	NR	1.17	0.22	0.051	0.073	NR
"	71	1755	1.5	"	"	"	"	1.25	0.33	0.044	0.073	NR	1.25	0.31	0.045	0.072	NR	1.17	0.22	0.051	0.073	NR
"	71	1800	1.5	"	"	"	"	1.25	0.33	0.044	0.073	NR	1.25	0.31	0.045	0.072	NR	1.17	0.22	0.051	0.073	NR
"	71	1805	1.5	"	"	"	"	1.25	0.33	0.044	0.073	NR	1.25	0.31	0.045	0.072	NR	1.17	0.22	0.051	0.073	NR
"	71	1810	1.5	"	"	"	"	1.25	0.33	0.044	0.073	NR	1.25	0.31	0.045	0.072	NR	1.17	0.22	0.051	0.073	NR
"	71	1815	1.5	"	"	"	"	1.25	0.33	0.044	0.073	NR	1.25	0.31	0.045	0.072	NR	1.17	0.22	0.051	0.073	NR
"	71	1820	1.5	"	"	"	"	1.25	0.33	0.044	0.073	NR	1.25	0.31	0.045	0.072	NR	1.17	0.22	0.051	0.073	NR
"	71	1825	1.5	"	"	"	"	1.25	0.33	0.044	0.073	NR	1.25	0.31	0.045	0.072	NR	1.17	0.22	0.051	0.073	NR
"	71	1830	1.5	"	"	"	"	1.25	0.33	0.044	0.073	NR	1.25	0.31	0.045	0.072	NR	1.17	0.22	0.051	0.073	NR
"	71	1835	1.5	"	"	"	"	1.25	0.33	0.044	0.073	NR	1.25	0.31	0.045	0.072	NR	1.17	0.22	0.051	0.073	NR
"	71	1840	1.5	"	"	"	"	1.25	0.33	0.044	0.073	NR	1.25	0.31	0.045	0.072	NR	1.17	0.22	0.051	0.073	NR
"	71	1845	1.5	"	"	"	"	1.25	0.33	0.044	0.073	NR	1.25	0.31	0.045	0.072	NR	1.17	0.22	0.051	0.073	NR
"	71	1850	1.5	"	"	"	"	1.25	0.33	0.044	0.073	NR	1.25	0.31	0.045	0.072	NR	1.17	0.22	0.051	0.073	NR
"	71	1855	1.5	"	"	"	"	1.25	0.33	0.044	0.073	NR	1.25	0.31	0.045	0.072	NR	1.17	0.22	0.051	0.073	NR
"	71	1900	1.5	"	"	"	"	1.25	0.33	0.044	0.073	NR	1.25	0.31	0.045	0.072	NR	1.17	0.22	0.051	0.073	NR
"	71	1905	1.5	"	"	"	"	1.25	0.33	0.044	0.073	NR	1.25	0.31	0.045	0.072	NR	1.17	0.22	0.051	0.073	NR
"	71	1910	1.5	"	"	"	"	1.25	0.33	0.044	0.073	NR	1.25	0.31	0.045	0.072	NR	1.17	0.22	0.051	0.073	NR
"	71	1915	1.5	"	"	"	"	1.25	0.33	0.044	0.073	NR	1.25	0.31	0.045	0.072	NR	1.17	0.22	0.051	0.073	NR
"	71	1920	1.5	"	"	"	"	1.25	0.33	0.044	0.073	NR	1.25	0.31	0.045	0.072	NR	1.17	0.22	0.051	0.073	NR
"	71	1925	1.5	"	"	"	"	1.25	0.33	0.044	0.073	NR	1.25	0.31	0.045	0.072	NR	1.17	0.22	0.051	0.073	NR
"	71	1930	1.5	"	"	"	"	1.25	0.33	0.044	0.073	NR	1.25	0.31	0.045	0.072	NR	1.17	0.22	0.051	0.073	NR
"	71	1935	1.5	"	"	"	"	1.25	0.33	0.044	0.073	NR	1.25	0.31	0.045	0.072	NR	1.17	0.22	0.051	0.073	NR
"	71	1940	1.5	"	"	"	"	1.25	0.33	0.044	0.073	NR	1.25	0.31	0.045	0.072	NR	1.17	0.22	0.051	0.073	NR
"	71	1945	1.5	"	"	"	"	1.25	0.33	0.044	0.073	NR	1.25	0.31	0.045	0.072	NR	1.17	0.22	0.051	0.073	NR
"	71	1950	1.5	"	"	"	"	1.25	0.33	0.044	0.073	NR	1.25	0.31	0.045	0.072	NR	1.17	0.22	0.051	0.073	NR
"	71	1955	1.5	"	"	"	"	1.25	0.33	0.044	0.073	NR	1.25	0.31	0.045	0.072	NR	1.17	0.22	0.051	0.073	NR
"	71	2000	1.5	"	"	"	"	1.25	0.33	0.044	0.073	NR	1.25	0.31	0.045	0.072	NR	1.17	0.22	0.051	0.073	NR
"	71	2005	1.5	"	"	"	"	1.25	0.33	0.044	0.073	NR	1.25	0.31	0.045	0.072	NR	1.17	0.22	0.051	0.073	NR
"	71	2010	1.5	"	"	"	"	1.25	0.33	0.044	0.073	NR	1.25	0.31	0.045	0.072	NR	1.17	0.22	0.051	0.073	NR
"	71	2015	1.5	"	"	"	"	1.25	0.33	0.044	0.073	NR	1.25	0.31	0.045	0.072	NR	1.17	0.22	0.051	0.073	NR
"	71	2020	1.5	"	"	"	"	1.2														

Table III.- Concluded.

OPERATING CONDITIONS				WEATHER				SONIC BOOM PRESSURE SIGNATURE DATA														
Date	Flight No.	Time	Mach No.	Surface Temp.	Surface Winds	Cloud Cover	Precipitation	Station 1					Station 3					Station 4				
								ΔP_0	ΔP_1	ΔI_0 Pos	I_0 Pos	Wave Shape	ΔP_0	ΔP_1	ΔI_0 Pos	I_0 Pos	Wave Shape	ΔP_0	ΔP_1	ΔI_0 Pos	I_0 Pos	Wave Shape
1-1-64	7-121	16:00	1.5	27°	300/10	☉	None	1.10	0.47	0.045	0.050	NH	0.43	0.26	0.045	0.050	NH	0.47	0.26	0.045	0.050	NH
1-1-64	8-122	16:01	1.5	"	"	"	"	1.14	0.47	0.039	0.051	NH	0.49	0.26	0.036	0.050	NH	0.47	0.26	0.036	0.050	NH
1-1-64	9-123	16:02	1.5	27°	120/10	"	"	1.03	0.38	0.05	0.056	NH	0.43	0.26	0.050	0.057	NH	0.47	0.26	0.050	0.057	NH
1-1-64	10-124	16:03	1.5	"	"	"	"	1.04	0.38	0.045	0.057	NH	0.39	0.26	0.050	0.057	NH	0.47	0.26	0.050	0.057	NH
1-1-64	11-125	16:04	1.5	"	"	"	"	1.07	0.37	0.047	0.058	NH	0.42	0.26	0.050	0.057	NH	0.47	0.26	0.050	0.057	NH
1-1-64	12-126	16:05	1.5	48°	130/15	☉	"	1.07	0.37	0.047	0.058	NH	0.42	0.26	0.050	0.057	NH	0.47	0.26	0.050	0.057	NH
1-1-64	13-127	16:06	1.5	"	"	"	"	1.08	0.37	0.047	0.058	NH	0.42	0.26	0.050	0.057	NH	0.47	0.26	0.050	0.057	NH
1-1-64	14-128	16:07	1.5	"	"	"	"	1.08	0.37	0.047	0.058	NH	0.42	0.26	0.050	0.057	NH	0.47	0.26	0.050	0.057	NH
1-1-64	15-129	16:08	1.5	"	"	"	"	1.08	0.37	0.047	0.058	NH	0.42	0.26	0.050	0.057	NH	0.47	0.26	0.050	0.057	NH
1-1-64	16-130	16:09	1.5	"	"	"	"	1.08	0.37	0.047	0.058	NH	0.42	0.26	0.050	0.057	NH	0.47	0.26	0.050	0.057	NH
1-1-64	17-131	16:10	1.5	"	"	"	"	1.08	0.37	0.047	0.058	NH	0.42	0.26	0.050	0.057	NH	0.47	0.26	0.050	0.057	NH
1-1-64	18-132	16:11	1.5	"	"	"	"	1.08	0.37	0.047	0.058	NH	0.42	0.26	0.050	0.057	NH	0.47	0.26	0.050	0.057	NH
1-1-64	19-133	16:12	1.5	"	"	"	"	1.08	0.37	0.047	0.058	NH	0.42	0.26	0.050	0.057	NH	0.47	0.26	0.050	0.057	NH
1-1-64	20-134	16:13	1.5	"	"	"	"	1.08	0.37	0.047	0.058	NH	0.42	0.26	0.050	0.057	NH	0.47	0.26	0.050	0.057	NH
1-1-64	21-135	16:14	1.5	"	"	"	"	1.08	0.37	0.047	0.058	NH	0.42	0.26	0.050	0.057	NH	0.47	0.26	0.050	0.057	NH
1-1-64	22-136	16:15	1.5	"	"	"	"	1.08	0.37	0.047	0.058	NH	0.42	0.26	0.050	0.057	NH	0.47	0.26	0.050	0.057	NH
1-1-64	23-137	16:16	1.5	"	"	"	"	1.08	0.37	0.047	0.058	NH	0.42	0.26	0.050	0.057	NH	0.47	0.26	0.050	0.057	NH
1-1-64	24-138	16:17	1.5	"	"	"	"	1.08	0.37	0.047	0.058	NH	0.42	0.26	0.050	0.057	NH	0.47	0.26	0.050	0.057	NH
1-1-64	25-139	16:18	1.5	"	"	"	"	1.08	0.37	0.047	0.058	NH	0.42	0.26	0.050	0.057	NH	0.47	0.26	0.050	0.057	NH
1-1-64	26-140	16:19	1.5	"	"	"	"	1.08	0.37	0.047	0.058	NH	0.42	0.26	0.050	0.057	NH	0.47	0.26	0.050	0.057	NH
1-1-64	27-141	16:20	1.5	"	"	"	"	1.08	0.37	0.047	0.058	NH	0.42	0.26	0.050	0.057	NH	0.47	0.26	0.050	0.057	NH
1-1-64	28-142	16:21	1.5	"	"	"	"	1.08	0.37	0.047	0.058	NH	0.42	0.26	0.050	0.057	NH	0.47	0.26	0.050	0.057	NH
1-1-64	29-143	16:22	1.5	"	"	"	"	1.08	0.37	0.047	0.058	NH	0.42	0.26	0.050	0.057	NH	0.47	0.26	0.050	0.057	NH
1-1-64	30-144	16:23	1.5	"	"	"	"	1.08	0.37	0.047	0.058	NH	0.42	0.26	0.050	0.057	NH	0.47	0.26	0.050	0.057	NH
1-1-64	31-145	16:24	1.5	"	"	"	"	1.08	0.37	0.047	0.058	NH	0.42	0.26	0.050	0.057	NH	0.47	0.26	0.050	0.057	NH
1-1-64	32-146	16:25	1.5	"	"	"	"	1.08	0.37	0.047	0.058	NH	0.42	0.26	0.050	0.057	NH	0.47	0.26	0.050	0.057	NH
1-1-64	33-147	16:26	1.5	"	"	"	"	1.08	0.37	0.047	0.058	NH	0.42	0.26	0.050	0.057	NH	0.47	0.26	0.050	0.057	NH
1-1-64	34-148	16:27	1.5	"	"	"	"	1.08	0.37	0.047	0.058	NH	0.42	0.26	0.050	0.057	NH	0.47	0.26	0.050	0.057	NH
1-1-64	35-149	16:28	1.5	"	"	"	"	1.08	0.37	0.047	0.058	NH	0.42	0.26	0.050	0.057	NH	0.47	0.26	0.050	0.057	NH
1-1-64	36-150	16:29	1.5	"	"	"	"	1.08	0.37	0.047	0.058	NH	0.42	0.26	0.050	0.057	NH	0.47	0.26	0.050	0.057	NH
1-1-64	37-151	16:30	1.5	"	"	"	"	1.08	0.37	0.047	0.058	NH	0.42	0.26	0.050	0.057	NH	0.47	0.26	0.050	0.057	NH
1-1-64	38-152	16:31	1.5	"	"	"	"	1.08	0.37	0.047	0.058	NH	0.42	0.26	0.050	0.057	NH	0.47	0.26	0.050	0.057	NH
1-1-64	39-153	16:32	1.5	"	"	"	"	1.08	0.37	0.047	0.058	NH	0.42	0.26	0.050	0.057	NH	0.47	0.26	0.050	0.057	NH
1-1-64	40-154	16:33	1.5	"	"	"	"	1.08	0.37	0.047	0.058	NH	0.42	0.26	0.050	0.057	NH	0.47	0.26	0.050	0.057	NH
1-1-64	41-155	16:34	1.5	"	"	"	"	1.08	0.37	0.047	0.058	NH	0.42	0.26	0.050	0.057	NH	0.47	0.26	0.050	0.057	NH
1-1-64	42-156	16:35	1.5	"	"	"	"	1.08	0.37	0.047	0.058	NH	0.42	0.26	0.050	0.057	NH	0.47	0.26	0.050	0.057	NH
1-1-64	43-157	16:36	1.5	"	"	"	"	1.08	0.37	0.047	0.058	NH	0.42	0.26	0.050	0.057	NH	0.47	0.26	0.050	0.057	NH
1-1-64	44-158	16:37	1.5	"	"	"	"	1.08	0.37	0.047	0.058	NH	0.42	0.26	0.050	0.057	NH	0.47	0.26	0.050	0.057	NH
1-1-64	45-159	16:38	1.5	"	"	"	"	1.08	0.37	0.047	0.058	NH	0.42	0.26	0.050	0.057	NH	0.47	0.26	0.050	0.057	NH
1-1-64	46-160	16:39	1.5	"	"	"	"	1.08	0.37	0.047	0.058	NH	0.42	0.26	0.050	0.057	NH	0.47	0.26	0.050	0.057	NH
1-1-64	47-161	16:40	1.5	"	"	"	"	1.08	0.37	0.047	0.058	NH	0.42	0.26	0.050	0.057	NH	0.47	0.26	0.050	0.057	NH
1-1-64	48-162	16:41	1.5	"	"	"	"	1.08	0.37	0.047	0.058	NH	0.42	0.26	0.050	0.057	NH	0.47	0.26	0.050	0.057	NH
1-1-64	49-163	16:42	1.5	"	"	"	"	1.08	0.37	0.047	0.058	NH	0.42	0.26	0.050	0.057	NH	0.47	0.26	0.050	0.057	NH
1-1-64	50-164	16:43	1.5	"	"	"	"	1.08	0.37	0.047	0.058	NH	0.42	0.26	0.050	0.057	NH	0.47	0.26	0.050	0.057	NH
1-1-64	51-165	16:44	1.5	"	"	"	"	1.08	0.37	0.047	0.058	NH	0.42	0.26	0.050	0.057	NH	0.47	0.26	0.050	0.057	NH
1-1-64	52-166	16:45	1.5	"	"	"	"	1.08	0.37	0.047	0.058	NH	0.42	0.26	0.050	0.057	NH	0.47	0.26	0.050	0.057	NH
1-1-64	53-167	16:46	1.5	"	"	"	"	1.08	0.37	0.047	0.058	NH	0.42	0.26	0.050	0.057	NH	0.47	0.26	0.050	0.057	NH
1-1-64	54-168	16:47	1.5	"	"	"	"	1.08	0.37	0.047	0.058	NH	0.42	0.26	0.050	0.057	NH	0.47	0.26	0.050	0.057	NH
1-1-64	55-169	16:48	1.5	"	"	"	"	1.08	0.37	0.047	0.058	NH	0.42	0.26	0.050	0.057	NH	0.47	0.26	0.050	0.057	NH
1-1-64	56-170	16:49	1.5	"	"	"	"	1.08	0.37	0.047	0.058	NH	0.42	0.26	0.050	0.057	NH	0.47	0.26	0.050	0.057	NH
1-1-64	57-171	16:50	1.5	"	"	"	"	1.08	0.37	0.047	0.058	NH	0.42	0.26	0.050	0.057	NH	0.47	0.26	0.050	0.057	NH
1-1-64	58-172	16:51	1.5	"	"	"	"	1.08	0.37	0.047	0.058	NH	0.42	0.26	0.050	0.057	NH	0.47	0.26	0.050	0.057	NH
1-1-64	59-173	16:52	1.5	"	"	"	"	1.08	0.37	0.047	0.058	NH	0.42	0.26	0.050	0.057	NH	0.47	0.26	0.050	0.057	NH
1-1-64	60-174	16:53	1.5	"	"	"	"	1.08	0.37	0.047	0.058	NH	0.42	0.26	0.050	0.057	NH	0.47	0.26	0.050	0.057	NH
1-1-64	61-175	16:54	1.5	"	"	"	"	1.08	0.37	0.047	0.058	NH	0.42	0.26	0.050	0.057	NH	0.47	0.26	0.050	0.057	NH
1-1-64	62-176	16:55	1.5	"	"	"	"	1.08	0.37	0.047	0.058	NH	0.42	0.26	0.050	0.057	NH	0.47	0.26	0.050	0.057	NH
1-1-64	63-177	16:56	1.5	"	"	"	"	1.08	0.37	0.047	0.058	NH	0.42	0.26	0.050	0.057	NH	0.47	0.26	0.050	0.057	NH
1-1-64	64-178	16:57	1.5	"	"	"	"	1.08	0.37	0.047	0.058	NH	0.42	0.26	0.050	0.057	NH	0.47	0.26	0.050	0.057	NH
1-1-64	65-179	16:58	1.5	"	"	"	"	1.08	0.37	0.047	0.058	NH	0.42	0.26	0.050	0.057	NH	0.47	0.26	0.050	0.057	NH
1-1-64	66-180	16:59	1.5	"	"	"	"	1.08	0.37	0.047	0.058	NH	0.42	0.26	0.050	0.057	NH	0.47	0.26	0.050	0.057	NH
1-1-64	67-181	17:00	1.5	"	"	"	"	1.08	0.37	0.047	0.058	NH	0.42	0.26	0.050	0.057	NH	0.47	0.26	0.050	0.057	NH
1-1-64	68-182	17:01	1.5	"	"																	

Table IV.- Summary Of Sonic Boom Data For Various Flights Of Airplane A
For An Altitude Of 31,000 Feet

OPERATING CONDITIONS				WEATHER			SONIC BOOM PRESSURE SIGNATURE DATA												
Date	Flight No.	Time	Mach No.	Surface Temp.	Surface Winds	Cloud Cover	Precipitation	Station 1				Station 3				Station 4			
								ΔP_0	ΔP_1	ΔP_2	Wave Shape	ΔP_0	ΔP_1	ΔP_2	Wave Shape	ΔP_0	ΔP_1	ΔP_2	Wave Shape
5/7/54	74	12:20	1.5	40°	17/15/10	I	None	1.05	0.38	0.047	R	1.14	0.39	0.045	NR	0.52	0.31	0.067	NR
5/7/54	74	12:20	1.5	40°	"	"	"	1.12	0.33	0.046	NR	1.21	0.36	0.045	NR	0.55	0.27	0.065	NR
5/7/54	74	12:20	1.5	40°	"	"	"	1.45	0.33	0.051	NR	1.53	0.35	0.049	NR	0.72	0.27	0.065	NR
5/7/54	74	12:20	1.5	40°	16/15/10	III	"	1.69	0.34	0.047	NR	1.03	0.33	0.039	NR	0.67	0.23	0.065	NR
5/7/54	74	12:20	1.5	40°	15/10/10	III	LW	1.43	0.26	0.044	NR	1.45	0.33	0.042	NR	0.64	0.23	0.065	NR
5/7/54	74	12:20	1.5	40°	"	"	"	1.71	0.20	0.046	R	1.74	0.26	0.037	NR	0.81	0.19	0.065	NR
5/7/54	74	12:20	1.5	40°	20/10/5	I	None	1.12	0.34	0.051	NR	1.38	0.30	0.047	NR	0.55	0.18	0.065	NR
5/7/54	74	12:20	1.5	40°	"	"	"	1.65	0.33	0.050	R	1.70	0.32	0.051	NR	0.82	0.18	0.065	NR
5/7/54	74	12:20	1.5	40°	30/10/10	O	"	1.38	0.45	0.048	N	1.24	0.34	0.041	NR	1.02	0.27	0.065	NR
5/7/54	74	12:20	1.5	40°	13/10/10	"	"	1.51	0.39	0.048	N	1.71	0.35	0.041	NR	1.40	0.27	0.065	NR
5/7/54	74	12:20	1.5	40°	"	"	"	1.88	0.41	0.046	NR	1.64	0.35	0.041	NR	1.13	0.27	0.065	NR
5/7/54	74	12:20	1.5	40°	"	"	"	1.94	0.47	0.046	NR	1.84	0.41	0.041	NR	1.04	0.27	0.065	NR
5/7/54	100	11:00	1.5	40°	30/10/15	"	"	1.68	0.47	0.051	R	0.97	0.34	0.042	NR	0.92	0.27	0.065	NR
5/7/54	101	11:11	1.5	40°	"	"	"	1.70	0.44	0.051	NR	1.05	0.34	0.042	NR	0.92	0.27	0.065	NR
5/7/54	102	11:01	1.5	40°	30/10/15	"	"	1.17	0.44	0.051	NR	1.03	0.34	0.042	NR	0.92	0.27	0.065	NR
5/7/54	103	11:00	1.5	40°	30/10/15	III	"	1.99	0.34	0.048	NR	1.30	0.34	0.042	NR	1.15	0.27	0.065	NR
5/7/54	104	11:20	1.5	40°	"	"	"	1.41	0.33	0.040	R	1.62	0.34	0.041	NR	1.18	0.27	0.065	NR

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Table V.- Summary Of Sonic Boom Data For Various Flights Of Airplane A

OPERATING CONDITIONS				WEATHER				SONIC BOOM PRESSURE SIGNATURE DATA														
Date	Flight No.	Time	Mach No.	Surface Temp.	Surface Winds	Cloud Cover	Precipitation	Station 1			Station 3			Station 4			Wave Shape					
								ΔP_1	ΔP_0	Δt_0	I_0	Wave Shape	ΔP_1	ΔP_0	Δt_0	I_0	Wave Shape	ΔP_1	ΔP_0	Δt_0	I_0	Wave Shape
11-11-51	1041	13:57	1.5	47	170/10	☉	None	0.33	1.10	0.040	0.005	N	0.41	1.15	0.045	0.007	N	0.35	1.10	0.035	0.005	N
"	"	14:02	1.5	35	240/100	☉	"	0.47	0.64	0.053	0.007	NK	0.33	1.05	0.045	0.009	NK	0.49	0.74	0.059	0.011	NK
11-12-51	1042	13:57	1.5	35	240/100	☉	"	0.44	1.18	0.058	0.005	N	0.35	1.05	0.049	0.011	NK	0.31	0.74	0.054	0.011	NK
"	"	14:00	1.5	42	230/10	☉	"	0.41	1.02	0.050	0.005	N	0.37	1.05	0.046	0.011	NK	0.33	0.74	0.054	0.011	NK
"	"	14:00	1.5	40	200/10	☉	"	0.47	1.36	0.046	0.005	N	0.47	1.05	0.046	0.011	NK	0.33	0.74	0.054	0.011	NK
"	"	14:00	1.5	40	200/10	☉	"	0.46	1.38	0.046	0.005	N	0.46	1.05	0.046	0.011	NK	0.33	0.74	0.054	0.011	NK
"	"	14:00	1.5	40	200/10	☉	"	0.46	1.17	0.046	0.005	N	0.46	1.05	0.046	0.011	NK	0.33	0.74	0.054	0.011	NK
"	"	14:00	1.5	40	200/10	☉	"	0.46	1.17	0.046	0.005	N	0.46	1.05	0.046	0.011	NK	0.33	0.74	0.054	0.011	NK
"	"	14:00	1.5	40	200/10	☉	"	0.46	1.17	0.046	0.005	N	0.46	1.05	0.046	0.011	NK	0.33	0.74	0.054	0.011	NK
"	"	14:00	1.5	40	200/10	☉	"	0.46	1.17	0.046	0.005	N	0.46	1.05	0.046	0.011	NK	0.33	0.74	0.054	0.011	NK
"	"	14:00	1.5	40	200/10	☉	"	0.46	1.17	0.046	0.005	N	0.46	1.05	0.046	0.011	NK	0.33	0.74	0.054	0.011	NK
"	"	14:00	1.5	40	200/10	☉	"	0.46	1.17	0.046	0.005	N	0.46	1.05	0.046	0.011	NK	0.33	0.74	0.054	0.011	NK
"	"	14:00	1.5	40	200/10	☉	"	0.46	1.17	0.046	0.005	N	0.46	1.05	0.046	0.011	NK	0.33	0.74	0.054	0.011	NK
"	"	14:00	1.5	40	200/10	☉	"	0.46	1.17	0.046	0.005	N	0.46	1.05	0.046	0.011	NK	0.33	0.74	0.054	0.011	NK
"	"	14:00	1.5	40	200/10	☉	"	0.46	1.17	0.046	0.005	N	0.46	1.05	0.046	0.011	NK	0.33	0.74	0.054	0.011	NK
"	"	14:00	1.5	40	200/10	☉	"	0.46	1.17	0.046	0.005	N	0.46	1.05	0.046	0.011	NK	0.33	0.74	0.054	0.011	NK
"	"	14:00	1.5	40	200/10	☉	"	0.46	1.17	0.046	0.005	N	0.46	1.05	0.046	0.011	NK	0.33	0.74	0.054	0.011	NK
"	"	14:00	1.5	40	200/10	☉	"	0.46	1.17	0.046	0.005	N	0.46	1.05	0.046	0.011	NK	0.33	0.74	0.054	0.011	NK
"	"	14:00	1.5	40	200/10	☉	"	0.46	1.17	0.046	0.005	N	0.46	1.05	0.046	0.011	NK	0.33	0.74	0.054	0.011	NK
"	"	14:00	1.5	40	200/10	☉	"	0.46	1.17	0.046	0.005	N	0.46	1.05	0.046	0.011	NK	0.33	0.74	0.054	0.011	NK
"	"	14:00	1.5	40	200/10	☉	"	0.46	1.17	0.046	0.005	N	0.46	1.05	0.046	0.011	NK	0.33	0.74	0.054	0.011	NK
"	"	14:00	1.5	40	200/10	☉	"	0.46	1.17	0.046	0.005	N	0.46	1.05	0.046	0.011	NK	0.33	0.74	0.054	0.011	NK
"	"	14:00	1.5	40	200/10	☉	"	0.46	1.17	0.046	0.005	N	0.46	1.05	0.046	0.011	NK	0.33	0.74	0.054	0.011	NK
"	"	14:00	1.5	40	200/10	☉	"	0.46	1.17	0.046	0.005	N	0.46	1.05	0.046	0.011	NK	0.33	0.74	0.054	0.011	NK
"	"	14:00	1.5	40	200/10	☉	"	0.46	1.17	0.046	0.005	N	0.46	1.05	0.046	0.011	NK	0.33	0.74	0.054	0.011	NK
"	"	14:00	1.5	40	200/10	☉	"	0.46	1.17	0.046	0.005	N	0.46	1.05	0.046	0.011	NK	0.33	0.74	0.054	0.011	NK
"	"	14:00	1.5	40	200/10	☉	"	0.46	1.17	0.046	0.005	N	0.46	1.05	0.046	0.011	NK	0.33	0.74	0.054	0.011	NK
"	"	14:00	1.5	40	200/10	☉	"	0.46	1.17	0.046	0.005	N	0.46	1.05	0.046	0.011	NK	0.33	0.74	0.054	0.011	NK
"	"	14:00	1.5	40	200/10	☉	"	0.46	1.17	0.046	0.005	N	0.46	1.05	0.046	0.011	NK	0.33	0.74	0.054	0.011	NK
"	"	14:00	1.5	40	200/10	☉	"	0.46	1.17	0.046	0.005	N	0.46	1.05	0.046	0.011	NK	0.33	0.74	0.054	0.011	NK
"	"	14:00	1.5	40	200/10	☉	"	0.46	1.17	0.046	0.005	N	0.46	1.05	0.046	0.011	NK	0.33	0.74	0.054	0.011	NK
"	"	14:00	1.5	40	200/10	☉	"	0.46	1.17	0.046	0.005	N	0.46	1.05	0.046	0.011	NK	0.33	0.74	0.054	0.011	NK
"	"	14:00	1.5	40	200/10	☉	"	0.46	1.17	0.046	0.005	N	0.46	1.05	0.046	0.011	NK	0.33	0.74	0.054	0.011	NK
"	"	14:00	1.5	40	200/10	☉	"	0.46	1.17	0.046	0.005	N	0.46	1.05	0.046	0.011	NK	0.33	0.74	0.054	0.011	NK
"	"	14:00	1.5	40	200/10	☉	"	0.46	1.17	0.046	0.005	N	0.46	1.05	0.046	0.011	NK	0.33	0.74	0.054	0.011	NK
"	"	14:00	1.5	40	200/10	☉	"	0.46	1.17	0.046	0.005	N	0.46	1.05	0.046	0.011	NK	0.33	0.74	0.054	0.011	NK
"	"	14:00	1.5	40	200/10	☉	"	0.46	1.17	0.046	0.005	N	0.46	1.05	0.046	0.011	NK	0.33	0.74	0.054	0.011	NK
"	"	14:00	1.5	40	200/10	☉	"	0.46	1.17	0.046	0.005	N	0.46	1.05	0.046	0.011	NK	0.33	0.74	0.054	0.011	NK
"	"	14:00	1.5	40	200/10	☉	"	0.46	1.17	0.046	0.005	N	0.46	1.05	0.046	0.011	NK	0.33	0.74	0.054	0.011	NK
"	"	14:00	1.5	40	200/10	☉	"	0.46	1.17	0.046	0.005	N	0.46	1.05	0.046	0.011	NK	0.33	0.74	0.054	0.011	NK
"	"	14:00	1.5	40	200/10	☉	"	0.46	1.17	0.046	0.005	N	0.46	1.05	0.046	0.011	NK	0.33	0.74	0.054	0.011	NK
"	"	14:00	1.5	40	200/10	☉	"	0.46	1.17	0.046	0.005	N	0.46	1.05	0.046	0.011	NK	0.33	0.74	0.054	0.011	NK
"	"	14:00	1.5	40	200/10	☉	"	0.46	1.17	0.046	0.005	N	0.46	1.05	0.046	0.011	NK	0.33	0.74	0.054	0.011	NK
"	"	14:00	1.5	40	200/10	☉	"	0.46	1.17	0.046	0.005	N	0.46	1.05	0.046	0.011	NK	0.33	0.74	0.054	0.011	NK
"	"	14:00	1.5	40	200/10	☉	"	0.46	1.17	0.046	0.005	N	0.46	1.05	0.046	0.011	NK	0.33	0.74	0.054	0.011	NK
"	"	14:00	1.5	40	200/10	☉	"	0.46	1.17	0.046	0.005	N	0.46	1.05	0.046	0.011	NK	0.33	0.74	0.054	0.011	NK
"	"	14:00	1.5	40	200/10	☉	"	0.46	1.17	0.046	0.005	N	0.46	1.05	0.046	0.011	NK	0.33	0.74	0.054	0.011	NK
"	"	14:00	1.5	40	200/10	☉	"	0.46	1.17	0.046	0.005	N	0.46	1.05	0.046	0.011	NK	0.33	0.74	0.054	0.011	NK
"	"	14:00	1.5	40	200/10	☉	"	0.46	1.17	0.046	0.005	N	0.46	1.05	0.046	0.011	NK	0.33	0.74	0.054	0.011	NK
"	"	14:00	1.5	40	200/10	☉	"	0.46	1.17	0.046	0.005	N	0.46	1.05	0.046	0.011	NK	0.33	0.74	0.054	0.011	NK
"	"	14:00	1.5	40	200/10	☉	"	0.46	1.17	0.046	0.005	N	0.46	1.05	0.046	0.011	NK	0.33	0.74	0.054	0.011	NK
"	"	14:00	1.5	40	200/10	☉	"	0.46	1.17	0.046	0.005	N	0.46	1.05	0.046	0.011	NK	0.33	0.74	0.054	0.011	NK
"	"	14:00	1.5	40	200/10	☉	"	0.46	1.17	0.046	0.005	N	0.46	1.05	0.046	0.011	NK	0.33	0.74	0.054	0.011	NK
"	"	14:00	1.5	40	200/10	☉	"	0.46	1.17	0.046	0.005	N	0.46	1.05	0.046	0.011	NK	0.33	0.74	0.054	0.011	NK
"	"	14:00	1.5	40	200/10	☉	"	0.46	1.17	0.046	0.005	N	0.46	1.05	0.046	0.011	NK	0.33	0.74	0.054	0.011	NK
"	"	14:00	1.5	40	200/10	☉	"	0.46	1.17	0.046	0.005	N	0.46	1.05	0.046	0.011	NK	0.33	0.74	0.054	0.011	NK
"	"	14:00	1.5	40	200/10	☉	"	0.46	1.17	0.046	0.005	N	0.46	1.05	0.046	0.011	NK	0.33	0.74	0.054	0.011	NK
"	"	14:00	1.5	40	200/10	☉	"	0.46	1.17	0.046	0.005	N	0.46	1.05	0.046	0.011	NK	0.33	0.74	0.054	0.011	NK
"	"	14:00	1.5	40	200/10	☉	"	0.46	1.17	0.046	0.005	N	0.46	1.05	0.046	0.011	NK	0.33	0.74	0.054	0.011	NK
"	"	14:00	1.5	40	200/10	☉	"	0.46	1.17	0.046	0.005	N	0.46	1.05	0.046	0.011	NK	0.33	0.74	0.054	0.011	NK
"	"	14:00	1.5	40	200/10	☉	"	0.46	1.17	0.046	0.005	N	0.46	1.05	0.046	0.011	NK	0.33	0.74	0.054	0.011	NK
"	"	14:00	1.5	40	200/10	☉	"	0.46	1.17	0.046	0.005	N	0.46	1.05	0.046	0.011	NK	0.33	0.74	0.054	0.011	NK

Table V.- Continued.

OPERATING CONDITIONS				WEATHER			SONIC BOOM PRESSURE SIGNATURE DATA												
Date	Flight No.	Time	Mach No.	Surface Temp.	Surface Winds	Cloud Cover	Precipitation	Station 1				Station 3				Station 4			
								ΔP_0	ΔP_1	ΔI_0	Wave Shape	ΔP_0	ΔP_1	ΔI_0	Wave Shape	ΔP_0	ΔP_1	ΔI_0	Wave Shape
15 May	4/200	7:00	1.7	45°	170/15	0	None	1.31	0.33	0.045	NP	1.32	0.45	0.025	NP	1.11	0.20	0.040	N
"	5/200	11:00	1.5	57°	170/15	"	"	1.31	.47	.051	NP	1.40	.42	.049	NP	1.46	.32	.026	N
"	6/204	11:00	1.7	"	"	"	"	1.47	.41	.050	NP	1.46	.42	.049	NP	.91	.32	.025	N
"	7/205	12:01	1.5	67°	170/15	0	"	.72	.46	.051	N	1.41	.47	.050	NP	1.69	.32	.026	N
"	8/206	12:00	1.7	"	"	"	"	.74	.42	.046	N	1.45	.42	.041	NP	1.85	.32	.026	N
"	9/207	13:00	1.5	45°	170/10	"	"	1.43	.44	.047	N	1.45	.41	.041	NP	.74	.32	.026	N
"	10/208	14:00	1.7	"	"	"	"	1.27	.41	.042	NP	1.45	.40	.040	NP	.74	.32	.026	N
"	11/209	15:00	1.7	"	155/10	0	"	1.67	.52	.047	NP	1.60	.51	.040	NP	.86	.32	.026	N
"	12/210	16:00	1.5	55°	170/15	"	"	1.15	.42	.047	NR	1.43	.44	.041	NR	.88	.32	.026	N
"	13/211	17:00	1.7	"	"	"	"	1.00	.43	.040	N	1.10	.37	.043	NR	1.82	.32	.026	N
"	14/212	18:00	1.7	45°	"	"	"	1.51	.45	.041	NR	1.61	.36	.038	NR	1.85	.32	.026	N
"	15/213	19:00	1.5	"	"	"	"	1.16	.41	.043	N	"	"	"	"	1.82	.32	.026	N
"	16/214	20:00	1.7	45°	170/15	0	"	1.43	.37	.040	N	1.34	.34	.039	NR	.77	.32	.026	N
"	17/215	21:00	1.5	60°	170/15	"	"	1.74	.27	.043	NR	1.61	.43	.044	NR	.55	.32	.026	N
"	18/216	22:00	1.7	"	185/10	"	"	1.07	.30	.040	NR	1.65	.44	.050	NR	.77	.32	.026	N
"	19/217	23:00	1.5	57°	170/10	0	"	1.14	.29	.044	NR	1.30	.39	.042	NR	.51	.32	.026	N
"	20/218	00:00	1.5	57°	"	0	"	1.12	.65	"	"	1.34	.40	.050	NR	.64	.32	.026	N
"	21/219	01:00	1.5	57°	"	0	"	1.06	.40	"	"	1.34	.40	.050	NR	.64	.32	.026	N
"	22/220	02:00	1.5	67°	180/10	"	"	1.47	.45	.043	NP	1.61	.37	.048	NR	.92	.32	.026	N
"	23/221	03:00	1.7	60°	180/10	"	"	1.30	.60	.049	NR	1.59	.36	.045	NR	.71	.32	.026	N
"	24/222	04:00	1.5	"	180/10	"	"	1.22	.71	.042	NR	1.67	.31	.043	NR	.84	.32	.026	N
"	25/223	05:00	1.7	60°	170/10	0	F	1.37	.52	.043	NP	1.30	.32	.040	NR	.69	.32	.026	N
"	26/224	06:00	1.5	"	"	0	"	1.35	.21	.039	NR	1.52	.72	.039	NR	.76	.32	.026	N
"	27/225	07:00	1.5	61°	170/10	0	None	1.02	.30	.044	NR	1.30	.42	.041	NR	.65	.32	.026	N
"	28/226	08:00	1.7	"	"	"	"	1.32	.71	.051	NR	1.30	.42	.041	NR	1.67	.32	.026	N
"	29/227	09:00	1.5	65°	180/10	"	"	.80	.55	.047	N	1.60	.33	.035	NR	.62	.32	.026	N
"	30/228	10:00	1.7	"	"	"	"	.80	.31	.047	NR	1.10	.33	.043	NR	.62	.32	.026	N
"	31/229	11:00	1.5	40°	170/15	0	L	1.25	.33	.040	NR	1.31	.41	.032	NR	.62	.32	.026	N
"	32/230	12:00	1.7	40°	170/15	0	L	1.25	.33	.040	NR	1.31	.41	.032	NR	.62	.32	.026	N
"	33/231	13:00	1.5	40°	170/15	0	L	1.25	.33	.040	NR	1.31	.41	.032	NR	.62	.32	.026	N
"	34/232	14:00	1.7	40°	170/15	0	L	1.25	.33	.040	NR	1.31	.41	.032	NR	.62	.32	.026	N
"	35/233	15:00	1.5	40°	170/15	0	L	1.25	.33	.040	NR	1.31	.41	.032	NR	.62	.32	.026	N
"	36/234	16:00	1.7	40°	170/15	0	L	1.25	.33	.040	NR	1.31	.41	.032	NR	.62	.32	.026	N
"	37/235	17:00	1.5	40°	170/15	0	L	1.25	.33	.040	NR	1.31	.41	.032	NR	.62	.32	.026	N
"	38/236	18:00	1.7	40°	170/15	0	L	1.25	.33	.040	NR	1.31	.41	.032	NR	.62	.32	.026	N
"	39/237	19:00	1.5	40°	170/15	0	L	1.25	.33	.040	NR	1.31	.41	.032	NR	.62	.32	.026	N
"	40/238	20:00	1.7	40°	170/15	0	L	1.25	.33	.040	NR	1.31	.41	.032	NR	.62	.32	.026	N
"	41/239	21:00	1.5	40°	170/15	0	L	1.25	.33	.040	NR	1.31	.41	.032	NR	.62	.32	.026	N
"	42/240	22:00	1.7	40°	170/15	0	L	1.25	.33	.040	NR	1.31	.41	.032	NR	.62	.32	.026	N
"	43/241	23:00	1.5	40°	170/15	0	L	1.25	.33	.040	NR	1.31	.41	.032	NR	.62	.32	.026	N
"	44/242	00:00	1.7	40°	170/15	0	L	1.25	.33	.040	NR	1.31	.41	.032	NR	.62	.32	.026	N
"	45/243	01:00	1.5	40°	170/15	0	L	1.25	.33	.040	NR	1.31	.41	.032	NR	.62	.32	.026	N
"	46/244	02:00	1.7	40°	170/15	0	L	1.25	.33	.040	NR	1.31	.41	.032	NR	.62	.32	.026	N
"	47/245	03:00	1.5	40°	170/15	0	L	1.25	.33	.040	NR	1.31	.41	.032	NR	.62	.32	.026	N
"	48/246	04:00	1.7	40°	170/15	0	L	1.25	.33	.040	NR	1.31	.41	.032	NR	.62	.32	.026	N
"	49/247	05:00	1.5	40°	170/15	0	L	1.25	.33	.040	NR	1.31	.41	.032	NR	.62	.32	.026	N
"	50/248	06:00	1.7	40°	170/15	0	L	1.25	.33	.040	NR	1.31	.41	.032	NR	.62	.32	.026	N
"	51/249	07:00	1.5	40°	170/15	0	L	1.25	.33	.040	NR	1.31	.41	.032	NR	.62	.32	.026	N
"	52/250	08:00	1.7	40°	170/15	0	L	1.25	.33	.040	NR	1.31	.41	.032	NR	.62	.32	.026	N
"	53/251	09:00	1.5	40°	170/15	0	L	1.25	.33	.040	NR	1.31	.41	.032	NR	.62	.32	.026	N
"	54/252	10:00	1.7	40°	170/15	0	L	1.25	.33	.040	NR	1.31	.41	.032	NR	.62	.32	.026	N
"	55/253	11:00	1.5	40°	170/15	0	L	1.25	.33	.040	NR	1.31	.41	.032	NR	.62	.32	.026	N
"	56/254	12:00	1.7	40°	170/15	0	L	1.25	.33	.040	NR	1.31	.41	.032	NR	.62	.32	.026	N
"	57/255	13:00	1.5	40°	170/15	0	L	1.25	.33	.040	NR	1.31	.41	.032	NR	.62	.32	.026	N
"	58/256	14:00	1.7	40°	170/15	0	L	1.25	.33	.040	NR	1.31	.41	.032	NR	.62	.32	.026	N
"	59/257	15:00	1.5	40°	170/15	0	L	1.25	.33	.040	NR	1.31	.41	.032	NR	.62	.32	.026	N
"	60/258	16:00	1.7	40°	170/15	0	L	1.25	.33	.040	NR	1.31	.41	.032	NR	.62	.32	.026	N
"	61/259	17:00	1.5	40°	170/15	0	L	1.25	.33	.040	NR	1.31	.41	.032	NR	.62	.32	.026	N
"	62/260	18:00	1.7	40°	170/15	0	L	1.25	.33	.040	NR	1.31	.41	.032	NR	.62	.32	.026	N
"	63/261	19:00	1.5	40°	170/15	0	L	1.25	.33	.040	NR	1.31	.41	.032	NR	.62	.32	.026	N
"	64/262	20:00	1.7	40°	170/15	0	L	1.25	.33	.040	NR	1.31	.41	.032	NR	.62	.32	.026	N
"	65/263	21:00	1.5	40°	170/15	0	L	1.25	.33	.040	NR	1.31	.41	.032	NR	.62	.32	.026	N
"	66/264	22:00	1.7	40°	170/15	0	L	1.25	.33	.040	NR	1.31	.41	.032	NR	.62	.32	.026	N
"	67/265	23:00	1.5	40°	170/15	0	L	1.25	.33	.040	NR	1.31	.41	.032	NR	.62	.32	.026	N
"	68/266	00:00	1.7	40°	170/15	0	L	1.25	.33	.040	NR	1.31	.41	.032	NR	.62	.32	.026	N
"	69/267	01:00	1.5	40°	170/15	0	L	1.25	.33	.040									

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Table V.- Continued.

Table V.- Concluded.

OPERATING CONDITIONS				WEATHER				SONIC BOOM PRESSURE SIGNATURE DATA											
Date	Flight No.	Time	Mach No.	Surface Temp.	Surface Winds	Cloud Cover	Precipitation	Station 1				Station 3				Station 4			
								ΔP_0	ΔP_1	ΔP_2	Wave Shape	ΔP_0	ΔP_1	ΔP_2	Wave Shape	ΔP_0	ΔP_1	ΔP_2	Wave Shape
10-1-64	1/101	7:00	1.5	52°	040/15	☉	None	1.04	-	-	N	1.07	-	-	NR	1.14	-	-	NR
"	1/102	7:10	1.7	52°	040/15	"	"	1.25	-	-	N	1.07	-	-	NR	1.07	-	-	NR
"	1/103	7:20	1.5	61°	040/15	"	"	1.16	-	-	N	1.24	-	-	NR	1.07	-	-	NR
"	1/104	7:30	1.7	70°	"	"	"	1.16	-	-	N	1.07	-	-	NR	1.07	-	-	NR
"	1/105	7:40	1.5	70°	"	"	"	1.26	-	-	NR	1.07	-	-	NR	1.07	-	-	NR
"	1/106	7:50	1.5	72°	140/10	"	"	1.19	-	-	NR	1.07	-	-	NR	1.07	-	-	NR
"	1/107	8:00	1.7	57°	120/15	"	"	1.03	-	-	NR	1.07	-	-	NR	1.07	-	-	NR
"	1/108	8:10	1.5	64°	"	"	"	1.07	-	-	NR	1.07	-	-	NR	1.07	-	-	NR
"	1/109	8:20	1.7	50°	040/15	"	None	1.24	-	-	NR	1.07	-	-	NR	1.07	-	-	NR
"	1/110	8:30	1.5	50°	040/15	"	"	1.07	-	-	NR	1.07	-	-	NR	1.07	-	-	NR
"	1/111	8:40	1.7	50°	040/15	"	"	1.11	-	-	NR	1.07	-	-	NR	1.07	-	-	NR
"	1/112	8:50	1.7	50°	040/15	"	"	1.12	-	-	NR	1.07	-	-	NR	1.07	-	-	NR
"	1/113	9:00	1.7	50°	040/15	"	"	1.06	-	-	NR	1.07	-	-	NR	1.07	-	-	NR
"	1/114	9:10	1.7	50°	040/15	"	"	1.07	-	-	NR	1.07	-	-	NR	1.07	-	-	NR
"	1/115	9:20	1.7	50°	040/15	"	"	1.14	-	-	NR	1.07	-	-	NR	1.07	-	-	NR
"	1/116	9:30	1.5	50°	040/15	"	"	1.14	-	-	NR	1.07	-	-	NR	1.07	-	-	NR
"	1/117	9:40	1.7	50°	040/15	"	"	1.14	-	-	NR	1.07	-	-	NR	1.07	-	-	NR
"	1/118	9:50	1.7	50°	040/15	"	"	1.14	-	-	NR	1.07	-	-	NR	1.07	-	-	NR
"	1/119	10:00	1.7	50°	040/15	"	"	1.14	-	-	NR	1.07	-	-	NR	1.07	-	-	NR
"	1/120	10:10	1.7	50°	040/15	"	"	1.14	-	-	NR	1.07	-	-	NR	1.07	-	-	NR
"	1/121	10:20	1.7	50°	040/15	"	"	1.14	-	-	NR	1.07	-	-	NR	1.07	-	-	NR
"	1/122	10:30	1.7	50°	040/15	"	"	1.14	-	-	NR	1.07	-	-	NR	1.07	-	-	NR
"	1/123	10:40	1.7	50°	040/15	"	"	1.14	-	-	NR	1.07	-	-	NR	1.07	-	-	NR
"	1/124	10:50	1.7	50°	040/15	"	"	1.14	-	-	NR	1.07	-	-	NR	1.07	-	-	NR
"	1/125	11:00	1.7	50°	040/15	"	"	1.14	-	-	NR	1.07	-	-	NR	1.07	-	-	NR
"	1/126	11:10	1.7	50°	040/15	"	"	1.14	-	-	NR	1.07	-	-	NR	1.07	-	-	NR
"	1/127	11:20	1.7	50°	040/15	"	"	1.14	-	-	NR	1.07	-	-	NR	1.07	-	-	NR
"	1/128	11:30	1.7	50°	040/15	"	"	1.14	-	-	NR	1.07	-	-	NR	1.07	-	-	NR
"	1/129	11:40	1.7	50°	040/15	"	"	1.14	-	-	NR	1.07	-	-	NR	1.07	-	-	NR
"	1/130	11:50	1.7	50°	040/15	"	"	1.14	-	-	NR	1.07	-	-	NR	1.07	-	-	NR
"	1/131	12:00	1.7	50°	040/15	"	"	1.14	-	-	NR	1.07	-	-	NR	1.07	-	-	NR
"	1/132	12:10	1.7	50°	040/15	"	"	1.14	-	-	NR	1.07	-	-	NR	1.07	-	-	NR
"	1/133	12:20	1.7	50°	040/15	"	"	1.14	-	-	NR	1.07	-	-	NR	1.07	-	-	NR
"	1/134	12:30	1.7	50°	040/15	"	"	1.14	-	-	NR	1.07	-	-	NR	1.07	-	-	NR
"	1/135	12:40	1.7	50°	040/15	"	"	1.14	-	-	NR	1.07	-	-	NR	1.07	-	-	NR
"	1/136	12:50	1.7	50°	040/15	"	"	1.14	-	-	NR	1.07	-	-	NR	1.07	-	-	NR
"	1/137	13:00	1.7	50°	040/15	"	"	1.14	-	-	NR	1.07	-	-	NR	1.07	-	-	NR
"	1/138	13:10	1.7	50°	040/15	"	"	1.14	-	-	NR	1.07	-	-	NR	1.07	-	-	NR
"	1/139	13:20	1.7	50°	040/15	"	"	1.14	-	-	NR	1.07	-	-	NR	1.07	-	-	NR
"	1/140	13:30	1.7	50°	040/15	"	"	1.14	-	-	NR	1.07	-	-	NR	1.07	-	-	NR
"	1/141	13:40	1.7	50°	040/15	"	"	1.14	-	-	NR	1.07	-	-	NR	1.07	-	-	NR
"	1/142	13:50	1.7	50°	040/15	"	"	1.14	-	-	NR	1.07	-	-	NR	1.07	-	-	NR
"	1/143	14:00	1.7	50°	040/15	"	"	1.14	-	-	NR	1.07	-	-	NR	1.07	-	-	NR
"	1/144	14:10	1.7	50°	040/15	"	"	1.14	-	-	NR	1.07	-	-	NR	1.07	-	-	NR
"	1/145	14:20	1.7	50°	040/15	"	"	1.14	-	-	NR	1.07	-	-	NR	1.07	-	-	NR
"	1/146	14:30	1.7	50°	040/15	"	"	1.14	-	-	NR	1.07	-	-	NR	1.07	-	-	NR
"	1/147	14:40	1.7	50°	040/15	"	"	1.14	-	-	NR	1.07	-	-	NR	1.07	-	-	NR
"	1/148	14:50	1.7	50°	040/15	"	"	1.14	-	-	NR	1.07	-	-	NR	1.07	-	-	NR
"	1/149	15:00	1.7	50°	040/15	"	"	1.14	-	-	NR	1.07	-	-	NR	1.07	-	-	NR
"	1/150	15:10	1.7	50°	040/15	"	"	1.14	-	-	NR	1.07	-	-	NR	1.07	-	-	NR
"	1/151	15:20	1.7	50°	040/15	"	"	1.14	-	-	NR	1.07	-	-	NR	1.07	-	-	NR
"	1/152	15:30	1.7	50°	040/15	"	"	1.14	-	-	NR	1.07	-	-	NR	1.07	-	-	NR
"	1/153	15:40	1.7	50°	040/15	"	"	1.14	-	-	NR	1.07	-	-	NR	1.07	-	-	NR
"	1/154	15:50	1.7	50°	040/15	"	"	1.14	-	-	NR	1.07	-	-	NR	1.07	-	-	NR
"	1/155	16:00	1.7	50°	040/15	"	"	1.14	-	-	NR	1.07	-	-	NR	1.07	-	-	NR
"	1/156	16:10	1.7	50°	040/15	"	"	1.14	-	-	NR	1.07	-	-	NR	1.07	-	-	NR
"	1/157	16:20	1.7	50°	040/15	"	"	1.14	-	-	NR	1.07	-	-	NR	1.07	-	-	NR
"	1/158	16:30	1.7	50°	040/15	"	"	1.14	-	-	NR	1.07	-	-	NR	1.07	-	-	NR
"	1/159	16:40	1.7	50°	040/15	"	"	1.14	-	-	NR	1.07	-	-	NR	1.07	-	-	NR
"	1/160	16:50	1.7	50°	040/15	"	"	1.14	-	-	NR	1.07	-	-	NR	1.07	-	-	NR
"	1/161	17:00	1.7	50°	040/15	"	"	1.14	-	-	NR	1.07	-	-	NR	1.07	-	-	NR
"	1/162	17:10	1.7	50°	040/15	"	"	1.14	-	-	NR	1.07	-	-	NR	1.07	-	-	NR
"	1/163	17:20	1.7	50°	040/15	"	"	1.14	-	-	NR	1.07	-	-	NR	1.07	-	-	NR
"	1/164	17:30	1.7	50°	040/15	"	"	1.14	-	-	NR	1.07	-	-	NR	1.07	-	-	NR
"	1/165	17:40	1.7	50°	040/15	"	"	1.14	-	-	NR	1.07	-	-	NR	1.07	-	-	NR
"	1/166	17:50	1.7	50°	040/15	"	"	1.14	-	-	NR	1.07	-	-	NR	1.07	-	-	NR
"	1/167	18:00	1.7	50°	040/15	"	"	1.14	-	-	NR	1.07	-	-	NR	1.07	-	-	NR
"	1/168	18:10	1.7	50°	040/15	"	"	1.14	-	-	NR	1.07	-	-	NR	1.07	-	-	NR
"	1/169	18:20	1.7	50°	040/15	"	"	1.14	-	-	NR	1.07	-	-	NR	1.07	-	-	NR
"	1/170	18:30	1.7	50°	040/15	"	"	1.14	-	-	NR	1.07	-	-	NR	1.07	-	-	NR
"	1/171	18:40	1.7	50°	040/15	"	"	1.14	-	-	NR	1.07	-	-	NR	1.07	-	-	NR
"	1/172	18:50	1.7	50°	040/15	"	"	1.14	-	-	NR	1.07							

Acoustic Boom Data For Various Flights Of Airplane A
For An Altitude Of 29,000 Feet

OPERATING CONDITIONS			WEATHER		SONIC BOOM PRESSURE SIGNATURE DATA																	
Date	Flight No.	Time	Mach No.	Surface Temp.	Surface Winds	Cloud Cover	Precipitation	Station 1				Station 3				Station 4						
								ΔP_0	ΔP_1	Δt_0 Pos.	I_0 Pos.	Wave Shape	ΔP_0	ΔP_1	Δt_0 Pos.	I_0 Pos.	Wave Shape	ΔP_0	ΔP_1	Δt_0 Pos.	I_0 Pos.	Wave Shape
3-1-64	3-112	7:00	1.5	36°	25/15-20	0	F	0.77	0.35	0.042	0.000	NR	0.64	0.27	0.050	0.019	NR	0.75	0.14	0.012	0.019	NR
3-1-64	4-215	7:00	1.7	40°	200/5	0	GF	1.15	0.35	0.041	0.017	NP	1.43	0.16	0.067	0.052	-	1.04	0.10	0.091	0.075	NR
3-1-64	5-201	7:00	1.7	36°	200/5	0		1.21	0.41	-	-	-	1.02	0.28	0.037	0.026	N	0.88	0.19	0.045	0.015	NR
3-1-64	6-211	7:00	1.5	36°	17-110	0	None	1.31	0.35	-	-	-	0.96	0.39	0.043	0.012	NR	0.66	0.22	0.052	0.002	NR
3-1-64	7-212	7:00	1.7	40°	200/5	0		1.75	0.41	0.046	0.002	-	1.36	0.46	0.041	0.062	NP	0.54	0.20	0.046	0.001	N
3-1-64	8-204	7:00	1.5	40°	200/5	0		1.18	0.35	0.043	0.002	N	1.31	0.46	0.042	0.084	NP	0.52	0.20	0.052	0.001	N
3-1-64	9-205	7:00	1.5	40°	170/15-20	0		1.73	0.41	0.051	0.002	NR	1.25	0.38	0.041	0.051	NR	0.41	0.20	0.045	0.001	N
3-1-64	10-206	7:00	1.7	40°	170/15-20	0		1.44	0.46	0.045	0.002	T	1.20	0.36	0.036	0.021	N	0.52	0.22	0.052	0.001	NR
3-1-64	11-207	7:00	1.5	40°	200/15	0		1.42	0.47	0.043	0.002	NP	1.24	0.37	0.047	0.025	N	0.52	0.22	0.052	0.001	NR
3-1-64	12-208	7:00	1.7	40°	200/15	0		1.28	0.44	0.046	0.002	NR	1.06	0.38	0.046	0.049	NR	0.54	0.22	0.052	0.001	NR
3-1-64	13-209	7:00	1.5	40°	200/15	0		1.41	0.47	0.044	0.002	NP	1.44	0.37	0.040	0.020	NR	0.54	0.22	0.052	0.001	NR
3-1-64	14-210	7:00	1.7	40°	200/15	0		1.67	0.47	0.042	0.002	T	1.16	0.44	0.040	0.022	NP	0.54	0.22	0.052	0.001	NR
3-1-64	15-211	7:00	1.5	40°	200/15	0		1.14	0.45	0.042	0.002	N	1.24	0.43	0.052	0.022	NR	0.54	0.22	0.052	0.001	NR
3-1-64	16-212	7:00	1.7	40°	200/15	0		1.66	0.45	0.041	0.002	NR	1.06	0.38	0.046	0.049	NR	0.54	0.22	0.052	0.001	NR
3-1-64	17-213	7:00	1.5	40°	200/15	0		1.30	0.47	0.042	0.002	NP	1.44	0.37	0.040	0.020	NR	0.54	0.22	0.052	0.001	NR
3-1-64	18-214	7:00	1.7	40°	200/15	0		1.69	0.47	0.042	0.002	N	1.16	0.44	0.040	0.022	NP	0.54	0.22	0.052	0.001	NR
3-1-64	19-215	7:00	1.5	40°	200/15	0		1.30	0.47	0.043	0.002	N	1.24	0.43	0.045	0.021	N	0.54	0.22	0.052	0.001	NR
3-1-64	20-216	7:00	1.7	40°	200/15	0		1.44	0.45	0.041	0.002	NP	1.24	0.43	0.047	0.021	N	0.54	0.22	0.052	0.001	NR
3-1-64	21-217	7:00	1.5	40°	200/15	0		1.29	0.45	0.042	0.002	NR	1.24	0.43	0.048	0.021	N	0.54	0.22	0.052	0.001	NR
3-1-64	22-218	7:00	1.7	40°	200/15	0		1.44	0.45	0.041	0.002	NR	1.24	0.43	0.048	0.021	N	0.54	0.22	0.052	0.001	NR
3-1-64	23-219	7:00	1.5	40°	200/15	0		1.29	0.45	0.042	0.002	NR	1.24	0.43	0.048	0.021	N	0.54	0.22	0.052	0.001	NR
3-1-64	24-220	7:00	1.7	40°	200/15	0		1.44	0.45	0.041	0.002	NR	1.24	0.43	0.048	0.021	N	0.54	0.22	0.052	0.001	NR
3-1-64	25-221	7:00	1.5	40°	200/15	0		1.29	0.45	0.042	0.002	NR	1.24	0.43	0.048	0.021	N	0.54	0.22	0.052	0.001	NR
3-1-64	26-222	7:00	1.7	40°	200/15	0		1.44	0.45	0.041	0.002	NR	1.24	0.43	0.048	0.021	N	0.54	0.22	0.052	0.001	NR
3-1-64	27-223	7:00	1.5	40°	200/15	0		1.29	0.45	0.042	0.002	NR	1.24	0.43	0.048	0.021	N	0.54	0.22	0.052	0.001	NR
3-1-64	28-224	7:00	1.7	40°	200/15	0		1.44	0.45	0.041	0.002	NR	1.24	0.43	0.048	0.021	N	0.54	0.22	0.052	0.001	NR
3-1-64	29-225	7:00	1.5	40°	200/15	0		1.29	0.45	0.042	0.002	NR	1.24	0.43	0.048	0.021	N	0.54	0.22	0.052	0.001	NR
3-1-64	30-226	7:00	1.7	40°	200/15	0		1.44	0.45	0.041	0.002	NR	1.24	0.43	0.048	0.021	N	0.54	0.22	0.052	0.001	NR
3-1-64	31-227	7:00	1.5	40°	200/15	0		1.29	0.45	0.042	0.002	NR	1.24	0.43	0.048	0.021	N	0.54	0.22	0.052	0.001	NR
3-1-64	32-228	7:00	1.7	40°	200/15	0		1.44	0.45	0.041	0.002	NR	1.24	0.43	0.048	0.021	N	0.54	0.22	0.052	0.001	NR
3-1-64	33-229	7:00	1.5	40°	200/15	0		1.29	0.45	0.042	0.002	NR	1.24	0.43	0.048	0.021	N	0.54	0.22	0.052	0.001	NR
3-1-64	34-230	7:00	1.7	40°	200/15	0		1.44	0.45	0.041	0.002	NR	1.24	0.43	0.048	0.021	N	0.54	0.22	0.052	0.001	NR
3-1-64	35-231	7:00	1.5	40°	200/15	0		1.29	0.45	0.042	0.002	NR	1.24	0.43	0.048	0.021	N	0.54	0.22	0.052	0.001	NR
3-1-64	36-232	7:00	1.7	40°	200/15	0		1.44	0.45	0.041	0.002	NR	1.24	0.43	0.048	0.021	N	0.54	0.22	0.052	0.001	NR
3-1-64	37-233	7:00	1.5	40°	200/15	0		1.29	0.45	0.042	0.002	NR	1.24	0.43	0.048	0.021	N	0.54	0.22	0.052	0.001	NR
3-1-64	38-234	7:00	1.7	40°	200/15	0		1.44	0.45	0.041	0.002	NR	1.24	0.43	0.048	0.021	N	0.54	0.22	0.052	0.001	NR
3-1-64	39-235	7:00	1.5	40°	200/15	0		1.29	0.45	0.042	0.002	NR	1.24	0.43	0.048	0.021	N	0.54	0.22	0.052	0.001	NR
3-1-64	40-236	7:00	1.7	40°	200/15	0		1.44	0.45	0.041	0.002	NR	1.24	0.43	0.048	0.021	N	0.54	0.22	0.052	0.001	NR
3-1-64	41-237	7:00	1.5	40°	200/15	0		1.29	0.45	0.042	0.002	NR	1.24	0.43	0.048	0.021	N	0.54	0.22	0.052	0.001	NR
3-1-64	42-238	7:00	1.7	40°	200/15	0		1.44	0.45	0.041	0.002	NR	1.24	0.43	0.048	0.021	N	0.54	0.22	0.052	0.001	NR
3-1-64	43-239	7:00	1.5	40°	200/15	0		1.29	0.45	0.042	0.002	NR	1.24	0.43	0.048	0.021	N	0.54	0.22	0.052	0.001	NR
3-1-64	44-240	7:00	1.7	40°	200/15	0		1.44	0.45	0.041	0.002	NR	1.24	0.43	0.048	0.021	N	0.54	0.22	0.052	0.001	NR
3-1-64	45-241	7:00	1.5	40°	200/15	0		1.29	0.45	0.042	0.002	NR	1.24	0.43	0.048	0.021	N	0.54	0.22	0.052	0.001	NR
3-1-64	46-242	7:00	1.7	40°	200/15	0		1.44	0.45	0.041	0.002	NR	1.24	0.43	0.048	0.021	N	0.54	0.22	0.052	0.001	NR
3-1-64	47-243	7:00	1.5	40°	200/15	0		1.29	0.45	0.042	0.002	NR	1.24	0.43	0.048	0.021	N	0.54	0.22	0.052	0.001	NR
3-1-64	48-244	7:00	1.7	40°	200/15	0		1.44	0.45	0.041	0.002	NR	1.24	0.43	0.048	0.021	N	0.54	0.22	0.052	0.001	NR
3-1-64	49-245	7:00	1.5	40°	200/15	0		1.29	0.45	0.042	0.002	NR	1.24	0.43	0.048	0.021	N	0.54	0.22	0.052	0.001	NR
3-1-64	50-246	7:00	1.7	40°	200/15	0		1.44	0.45	0.041	0.002	NR	1.24	0.43	0.048	0.021	N	0.54	0.22	0.052	0.001	NR
3-1-64	51-247	7:00	1.5	40°	200/15	0		1.29	0.45	0.042	0.002	NR	1.24	0.43	0.048	0.021	N	0.54	0.22	0.052	0.001	NR
3-1-64	52-248	7:00	1.7	40°	200/15	0		1.44	0.45	0.041	0.002	NR	1.24	0.43	0.048	0.021	N	0.54	0.22	0.052	0.001	NR
3-1-64	53-249	7:00	1.5	40°	200/15	0		1.29	0.45	0.042	0.002	NR	1.24	0.43	0.048	0.021	N	0.54	0.22	0.052	0.001	NR
3-1-64	54-250	7:00	1.7	40°	200/15	0		1.44	0.45	0.041	0.002	NR	1.24	0.43	0.048	0.021	N	0.54	0.22	0.052	0.001	NR
3-1-64	55-251	7:00	1.5	40°	200/15	0		1.29	0.45	0.042	0.002	NR	1.24	0.43	0.048	0.021	N	0.54	0.22	0.052	0.001	NR
3-1-64	56-252	7:00	1.7	40°	200/15	0		1.44	0.45	0.041	0.002	NR	1.24	0.43	0.048	0.021	N	0.54	0.22	0.052	0.001	NR
3-1-64	57-253	7:00	1.5	40°	200/15	0		1.29	0.45	0.042	0.002	NR	1.24	0.43	0.048	0.021	N	0.54	0.22	0.052	0.001	NR
3-1-64	58-254	7:00	1.7	40°	200/15	0		1.44	0.45	0.041	0.002	NR	1.24	0.43	0.048	0.021	N	0.54	0.22	0.052	0.001	NR
3-1-64	59-255	7:00	1.5	40°	200/15	0		1.29	0.45	0.042	0.002	NR	1.24	0.43	0.048	0.021	N	0.54	0.22	0.052	0.001	NR
3-1-64	60-256	7:00	1.7	40°	200/15	0		1.44	0.45	0.041	0.002	NR	1.24	0.43	0.048	0.021	N	0.54	0.22	0.052	0.001	NR
3-1-64	61-257	7:00	1.5	40°	200/15	0		1.29	0.45	0.042	0.002	NR	1.24	0.43	0.048	0.021	N	0.54	0.22	0.052	0.001	NR
3-1-64	62-258	7:00																				

Table VI.- Continued.

OPERATING CONDITIONS				WEATHER				SONIC BOOM PRESSURE SIGNATURE DATA											
Date	Flight No.	Time	Mach No.	Surface Temp.	Surface Winds	Cloud Cover	Precipitation	Station 1				Station 3				Station 4			
								ΔP_1	ΔP_0	Wave Shape	ΔP_1	ΔP_0	Wave Shape	ΔP_1	ΔP_0	Wave Shape	ΔP_1	ΔP_0	Wave Shape
2-14-64	1/252	7:01	1.5	40°	300/1000	☉	None	0.41	1.16	NP	0.36	1.28	NP	0.36	1.28	T	0.19	0.57	0.015
"	2/254	7:19	1.7	"	"	"	"	0.34	1.28	NP	0.46	1.42	NP	0.46	1.42	NR	0.37	1.19	0.014
"	3/254	7:00	1.5	40°	340/1500	☉	"	0.35	1.09	N	0.30	1.29	NR	0.45	1.15	NR	0.37	1.15	0.012
"	4/255	7:20	1.7	"	"	☉	"	0.40	1.16	NR	0.41	1.34	NR	0.41	1.34	NP	0.36	1.15	0.012
"	5/256	11:00	1.5	55°	300/1000	☉	"	0.44	1.32	N	0.34	1.12	N	0.44	1.12	NP	0.16	0.40	0.014
"	6/257	11:19	1.7	"	"	"	"	0.38	1.15	RP	0.45	1.25	RP	0.37	1.25	P	0.32	1.27	0.017
"	7/257	13:27	1.5	"	"	☉	"	0.50	1.24	RP	0.48	1.10	RP	0.38	1.08	P	0.36	1.08	0.017
"	8/258	13:30	1.7	35°	230/5	☉	"	0.39	1.17	N	0.35	1.09	N	0.42	1.09	P	0.35	1.09	0.017
"	1/259	7:00	1.5	"	"	"	"	0.44	1.17	N	0.44	1.41	N	0.44	1.41	NR	0.35	1.01	0.017
"	2/260	7:19	1.7	"	"	"	"	0.44	1.17	N	0.44	1.41	N	0.44	1.41	NR	0.35	1.01	0.017
"	3/261	7:00	1.5	35°	270/4	"	"	0.44	1.48	N	0.44	1.48	N	0.44	1.48	N	0.44	1.48	0.017
"	4/262	7:19	1.7	40°	170/5	☉	"	0.50	1.12	N	0.44	1.41	N	0.44	1.41	N	0.44	1.41	0.017
"	5/263	7:00	1.7	30°	350/1000	☉	S	0.50	1.14	NR	0.44	1.31	NR	0.44	1.31	NR	0.44	1.31	0.017
"	6/264	7:19	1.55	30°	350/1000	☉	"	0.48	1.19	R	0.48	1.45	R	0.48	1.45	NR	0.44	1.45	0.017
2-14-64	7/261	13:30	1.7	45°	350/10	☉	None	0.47	1.10	NR	0.44	1.39	NR	0.44	1.39	NR	0.44	1.39	0.017
"	8/262	7:00	1.5	25°	180/10	1-☉	"	0.48	1.09	NR	0.44	1.17	NR	0.44	1.17	NR	0.44	1.17	0.017
"	9/263	7:19	1.7	"	"	"	"	0.44	1.24	N	0.44	1.30	N	0.44	1.30	N	0.44	1.30	0.017
"	10/264	7:00	1.5	50°	300/10	☉	"	0.45	1.11	NR	0.44	1.25	NR	0.44	1.25	NR	0.44	1.25	0.017
"	11/265	7:19	1.5	"	"	"	"	0.44	1.06	NR	0.44	1.40	NR	0.44	1.40	NR	0.44	1.40	0.017
"	12/266	7:00	1.5	27°	"	"	"	0.45	1.02	NR	0.44	1.32	NR	0.44	1.32	NR	0.44	1.32	0.017
"	13/267	11:00	1.5	40°	"	"	"	0.46	1.10	NR	0.44	1.30	NR	0.44	1.30	NR	0.44	1.30	0.017
"	14/268	13:00	1.5	60°	"	"	"	0.50	1.14	NR	0.44	1.32	NR	0.44	1.32	NR	0.44	1.32	0.017
"	15/269	13:17	1.7	"	"	"	"	0.51	1.02	NR	0.44	1.10	NR	0.44	1.10	NR	0.44	1.10	0.017

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[illegible]

Table VII.- Continued.

SONIC BOOM PRESSURE SIGNATURE DATA																						
OPERATING CONDITIONS				WEATHER			STATION 3						STATION 4									
Date	Flight No.	Time	Mach No.	Surface Temp.	Surface Winds	Cloud Cover	Precipitation	ΔP_0	ΔP_1	ΔI_0 Pos.	I_0 Pos.	Wave Shape	ΔP_0	ΔP_1	ΔI_0 Pos.	I_0 Pos.	Wave Shape	ΔP_0	ΔP_1	ΔI_0 Pos.	I_0 Pos.	Wave Shape
4-10-64	1/401	659	1.5	56°	170/10	0	None	1.11	-	0.043	0.003	N	1.13	-	0.043	0.004	N	1.08	-	0.040	0.010	N
"	2/400	719	1.7	55°	190/15+55	"	"	1.57	-	0.04	0.021	NR	1.14	-	0.040	0.048	NR	1.08	-	0.041	0.043	NR
"	3/401	760	1.5	55°	"	"	"	.96	-	0.01	0.004	NR	1.34	-	0.040	0.035	NR	1.17	-	0.041	0.017	NR
"	4/400	719	1.7	70°	110/15+55	"	"	.96	-	0.05	0.025	NR	1.91	-	0.037	0.075	NR	.65	-	0.046	0.070	NR
"	5/401	1100	1.5	70°	"	"	"	.77	-	0.07	0.016	NR	1.41	-	0.058	0.058	NR	1.36	-	0.043	0.085	NR
"	6/400	1113	1.7	70°	"	"	"	.77	-	0.07	0.016	NR	1.53	-	0.058	0.063	NR	.59	-	0.051	0.071	NR
"	7/400	1200	1.5	"	"	"	"	.57	-	0.045	0.013	NR	1.38	-	0.039	0.050	N	1.06	-	0.048	0.034	N
"	8/400	1217	1.7	"	"	"	"	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
"	1/401	659	1.5	45°	360/15+55	0	"	1.40	-	0.06	0.010	N	1.98	-	0.040	0.067	NR	.55	-	0.051	0.040	NR
"	2/400	719	1.7	45°	"	0	"	1.55	-	0.06	0.009	N	.99	-	0.058	0.058	NR	.86	-	0.049	0.047	NR
"	3/401	760	1.5	45°	"	0	"	1.17	-	0.06	0.014	NR	1.06	-	0.037	0.073	NR	.25	-	0.040	0.077	NR
"	4/400	719	1.7	47°	360/15+55	0	"	1.15	-	0.04	0.014	NR	1.75	-	0.036	0.054	NR	.94	-	0.036	0.073	NR
"	5/401	1100	1.5	47°	"	0	"	1.11	-	0.04	0.014	NR	1.94	-	0.036	0.064	NR	1.54	-	0.041	0.041	NR
"	6/400	1113	1.7	"	360/15+55	"	"	1.45	-	0.03	0.011	NR	1.91	-	0.040	0.037	NR	1.48	-	0.038	0.045	NR
"	7/400	1200	1.5	"	"	"	"	1.65	-	0.04	0.015	NR	1.47	-	0.041	0.043	NR	1.15	-	0.051	0.045	NR
"	8/400	1217	1.7	"	"	"	"	1.73	-	0.06	0.015	NR	1.33	-	0.045	0.074	N	.83	-	0.057	0.043	N
4-10-64	1/401	760	1.5	49°	250/10	0	"	1.09	-	0.04	0.031	NR	1.16	-	0.036	0.083	NR	.67	-	0.041	0.051	NR
"	2/400	719	1.7	51°	"	"	"	1.55	-	0.039	0.010	N	1.33	-	0.041	0.046	NR	1.13	-	0.039	0.067	NR
"	3/401	760	1.5	51°	"	"	"	.86	-	0.04	0.019	NR	1.32	-	0.045	0.039	NR	1.08	-	0.040	0.074	NR
"	4/400	1100	1.5	45°	360/15	"	"	1.52	0.73	0.04	0.019	NR	1.14	-	0.040	0.093	NR	1.04	-	0.045	0.046	NR
"	5/401	1113	1.7	51°	"	"	"	1.00	.90	0.04	0.015	NR	1.77	-	0.039	0.085	NR	.77	-	0.049	0.059	NR
"	6/400	1200	1.5	51°	360/15+55	"	"	1.59	.83	0.04	0.015	NR	1.65	-	0.040	0.074	NR	.85	-	0.056	0.048	NR
"	7/400	1217	1.7	"	"	"	"	1.38	-	0.04	0.019	NR	1.38	-	0.040	0.079	NR	1.05	-	0.056	0.084	NR
4-10-64	1/401	760	1.5	52°	190/10	"	"	1.48	-	0.04	0.017	NR	1.05	-	0.040	0.073	N	.83	-	0.048	0.073	N
"	2/400	719	1.7	46°	190/15	"	"	1.17	.94	0.03	0.033	NR	1.27	-	0.039	0.073	NR	.91	-	0.038	0.073	NR
"	3/401	760	1.5	51°	"	"	"	1.31	.79	0.04	0.017	NR	1.14	-	0.045	0.051	NR	1.04	-	0.040	0.072	NR
"	4/400	1100	1.5	51°	110/15	"	"	1.75	.87	0.04	0.017	NR	1.31	-	0.045	0.064	NR	.77	-	0.045	0.070	NR
"	5/401	1113	1.7	51°	"	"	"	1.01	.74	0.04	0.017	NR	1.06	-	0.040	0.064	NR	1.06	-	0.045	0.073	NR
"	6/400	1200	1.5	51°	"	"	"	1.15	.83	0.04	0.017	NR	.54	-	0.030	0.067	NR	.31	-	0.062	0.067	NR
"	7/400	1217	1.7	"	"	"	"	1.10	.77	0.04	0.017	NR	1.14	-	0.049	0.059	NR	.54	-	0.051	0.067	NR
4-10-64	1/401	760	1.5	44°	170/10	0	"	1.12	.83	0.04	0.017	NR	1.47	-	0.055	0.048	NR	.76	-	0.046	0.073	NR
"	2/400	719	1.7	55°	170/15+55	0	"	1.55	.87	0.04	0.017	NR	1.49	-	0.046	0.087	NR	.87	-	0.050	0.073	NR
"	3/401	760	1.5	"	"	"	"	1.14	.61	0.04	0.017	NR	1.10	-	0.046	0.071	N	1.10	-	0.037	0.073	N

Table VII.- Continued.

OPERATING CONDITIONS				WEATHER			SONIC BOOM PRESSURE SIGNATURE DATA															
Date	Flight No.	Time	Mach No.	Surface Temp.	Surface Winds	Cloud Cover	Precipitation	Station 1				Station 3				Station 4						
								ΔP_0	ΔP_1	Δt_0 Pos.	I_0 Pos.	Wave Shape	ΔP_0	ΔP_1	Δt_0 Pos.	I_0 Pos.	Wave Shape	ΔP_0	ΔP_1	Δt_0 Pos.	I_0 Pos.	Wave Shape
4-11-64	1/474	7:40	1.5	55°	150/1405	0	None	1.01	-	0.049	0.000	NR	1.14	-	0.048	0.017	R	0.27	-	0.046	0.000	R
"	2/475	7:40	1.5	69°	"	1	"	.87	-	0.048	0.024	NR	1.04	-	0.042	0.034	R	.97	-	0.046	0.017	R
"	3/476	7:40	1.5	"	150/1400	1	"	.85	-	0.054	0.066	NR	1.53	-	0.071	0.071	N	.55	-	0.052	0.012	N
"	4/477	7:40	1.5	74°	"	1	"	.81	-	0.057	0.045	NR	1.55	-	0.047	0.061	N	1.02	-	0.048	0.043	N
"	5/478	7:40	1.5	"	"	1	"	.82	-	0.051	0.065	NR	1.04	-	0.055	0.045	C	.31	-	0.048	0.049	C
"	6/479	7:40	1.5	75°	"	"	"	.75	-	0.049	0.050	NR	1.53	-	0.050	0.046	NP	.70	-	0.050	0.010	NP
"	7/480	7:40	1.5	"	"	"	"	.73	-	0.048	0.061	NR	1.15	-	0.043	0.063	NR	.40	-	0.050	0.060	NR
"	8/481	7:40	1.5	"	"	"	"	1.16	-	0.051	0.057	NR	1.10	-	0.051	0.061	NR	.57	-	0.050	0.060	NR
"	9/482	7:40	1.5	65°	170/1405	0	"	1.21	-	0.047	0.055	NP	1.97	-	0.043	0.066	NP	.44	-	0.047	0.043	NP
"	10/483	7:40	1.5	"	"	1	"	1.13	-	0.045	0.045	NP	1.55	-	0.044	0.061	N	.49	-	0.046	0.050	N
"	11/484	7:40	1.5	67°	170/1405	1	"	1.13	-	0.044	0.044	NP	1.16	-	0.044	0.036	N	1.06	-	0.048	0.041	N
"	12/485	7:40	1.5	"	"	"	"	1.11	-	0.040	0.051	P	.51	-	0.059	0.057	N	.65	-	0.052	0.061	N
"	13/486	7:40	1.5	75°	170/1405	"	"	.92	-	0.041	0.065	N	1.32	-	0.051	0.033	C	1.39	-	0.032	0.060	C
"	14/487	7:40	1.5	"	"	"	"	.85	-	0.053	0.055	NR	.96	-	0.047	0.043	NR	.49	-	0.066	0.048	NR
"	15/488	7:40	1.5	67°	170/1400	0	F	.74	-	0.045	0.078	NR	1.38	-	0.041	0.010	NP	-	-	-	-	-
"	16/489	7:40	1.5	"	"	"	None	1.03	-	0.052	0.036	NR	1.81	-	0.041	0.026	NP	-	-	-	-	-
"	17/490	7:40	1.5	70°	150/1405	"	"	.90	-	0.047	0.094	NR	1.22	-	0.048	0.049	NR	-	-	-	-	-
"	18/491	7:40	1.5	"	"	"	"	.56	-	0.050	0.064	R	1.51	-	0.046	0.033	N	-	-	-	-	-
"	19/492	7:40	1.5	75°	"	"	"	.95	-	0.050	0.060	R	1.40	-	0.047	0.054	C	.87	-	0.051	0.064	C
"	20/493	7:40	1.5	"	"	"	"	.66	-	0.053	0.065	NR	.78	-	0.045	0.054	C	.96	-	0.051	0.067	C
"	21/494	7:40	1.5	"	"	"	"	1.09	-	0.049	0.053	NR	1.04	-	0.045	0.049	C	.55	-	0.051	0.067	C
"	22/495	7:40	1.5	"	"	"	"	1.05	-	0.050	0.049	NR	1.19	-	0.050	0.048	R	.51	-	0.064	0.060	R
"	23/496	7:40	1.5	68°	170/1400	0	L	.88	-	0.049	0.087	NR	.54	-	0.044	0.022	P	.62	-	0.048	0.063	P
"	24/497	7:40	1.5	69°	"	"	None	1.06	-	0.048	0.048	NR	1.90	-	0.047	0.067	P	.69	-	0.049	0.060	P
"	25/498	7:40	1.5	"	150/1405	"	"	1.00	-	0.048	0.068	NR	1.01	-	0.051	0.022	R	.51	-	0.051	0.061	R
"	26/499	7:40	1.5	71°	"	"	"	.96	-	0.044	0.038	P	1.74	-	0.053	0.026	P	.50	-	0.053	0.065	P
"	27/500	7:40	1.5	"	170/1400	"	"	.78	-	0.048	0.048	NR	1.12	-	0.047	0.049	NR	.42	-	0.048	0.062	NR
"	28/501	7:40	1.5	74°	"	"	"	.78	-	0.046	0.061	NR	1.57	-	0.052	0.029	NR	.55	-	0.044	0.065	NR
"	29/502	7:40	1.5	"	"	"	"	1.06	-	0.047	0.050	P	.65	-	0.046	0.030	P	.52	-	0.054	0.064	P
"	30/503	7:40	1.5	"	"	"	"	1.04	-	0.049	0.052	NR	1.72	-	0.047	0.012	NR	.71	-	0.052	0.067	NR
"	31/504	7:40	1.5	70°	170/1405	0	"	.75	-	0.048	0.086	R	1.18	-	0.045	0.057	NR	-	-	-	-	-
"	32/505	7:40	1.5	"	"	"	"	1.02	-	0.047	0.047	NR	1.57	-	0.046	0.027	NR	-	-	-	-	-
"	33/506	7:40	1.5	"	170/1405	"	"	.67	-	0.045	0.043	R	.61	-	0.054	0.012	R	-	-	-	-	-
"	34/507	7:40	1.5	"	"	"	"	.77	-	0.050	0.045	R	.73	-	0.047	0.023	R	-	-	-	-	-

Table VII.- Continued.

OPERATING CONDITIONS				WEATHER				SONIC BOOM PRESSURE SIGNATURE DATA																	
Date	Flight No.	Time	Mach No.	Surface Temp.	Surface Winds	Cloud Cover	Precipitation	Station 1				Station 3				Station 4									
								ΔP_0	ΔP_1	Δt_0 Pos	I_0 Pos	Wave Shape	ΔP_0	ΔP_1	Δt_0 Pos	I_0 Pos	Wave Shape	ΔP_0	ΔP_1	Δt_0 Pos	I_0 Pos	Wave Shape			
4-12-64	4/424	911	1.5	53°	180/1000	0	None	0.15	0.51	0.051	0.059	R	1.15	-	0.044	0.053	0.053	0.053	NP	1.13	-	0.051	0.053	0.053	NP
"	5/425	1100	1.5	65°	100/1500	"	"	.85	.46	.050	.048	NR	1.98	-	.050	.051	.051	.051	NR	.51	-	.046	.046	.046	NR
"	6/426	1114	1.5	51°	170/1000	0	"	1.80	.75	.050	.043	-	1.34	-	.054	.054	.054	.054	NR	1.34	-	.046	.046	.046	NR
4-11-64	4/427	1100	1.5	60°	"	0	Hail	1.03	.75	.045	.073	NR	1.08	-	.045	.074	.074	.074	-	.74	-	.045	.047	.047	NR
"	5/428	1114	1.5	60°	"	"	"	1.10	.74	.046	.073	NR	1.31	-	.046	.074	.074	.074	NR	.83	-	.051	.051	.051	NR
"	6/429	1200	1.5	65°	100/1000	0	None	1.62	.71	.044	.073	NR	1.87	-	.040	.073	.073	.073	NR	1.04	-	.051	.051	.051	NR
"	7/430	1200	1.5	65°	"	"	"	1.62	.71	.044	.073	NR	1.87	-	.040	.073	.073	.073	NR	1.04	-	.051	.051	.051	NR
"	1/440	700	1.5	57°	170/115	"	F	1.21	.83	.044	.055	NR	1.18	-	.045	.073	.073	.073	NR	.66	-	.051	.051	.051	NR
"	3/441	750	1.5	"	"	"	"	1.00	.74	.045	.055	NR	1.28	-	.040	.073	.073	.073	NR	.61	-	.051	.051	.051	NR
"	4/442	700	1.5	65°	180/115	0	None	1.06	.59	.050	.064	NR	1.29	-	.050	.073	.073	.073	NR	1.28	-	.051	.051	.051	NR
"	4/443	920	1.5	"	"	"	"	.82	.50	.051	.063	R	.78	-	.045	.073	.073	.073	NR	1.26	-	.051	.051	.051	NR
"	5/450	1104	1.5	75°	100/1500	"	"	1.25	.51	.043	.055	NR	1.14	-	.045	.073	.073	.073	NR	1.33	-	.051	.051	.051	NR
"	6/451	1119	1.5	"	"	"	"	1.26	.79	.045	.055	NR	1.44	-	.047	.073	.073	.073	NR	1.33	-	.046	.046	.046	NR
"	7/452	1259	1.5	85°	100/1000	"	"	.86	.57	.050	.073	R	1.18	-	.053	.073	.073	.073	NR	1.25	-	.062	.062	.062	NR
"	8/453	1320	1.5	"	"	"	"	.73	.62	.049	.073	R	1.14	-	.053	.073	.073	.073	NR	1.25	-	.062	.062	.062	NR
4-12-64	1/454	659	1.5	59°	300/1	0	"	1.24	.56	.042	.045	NR	1.03	-	.039	.070	.070	.070	NR	.85	-	.036	.036	.036	NR
"	2/455	719	1.5	"	310/1000	"	"	1.26	.51	.043	.045	NR	1.36	-	.038	.070	.070	.070	NR	.99	-	.043	.043	.043	NR
"	3/456	700	1.5	58°	"	"	"	1.26	.59	.043	.045	NR	1.38	-	.040	.070	.070	.070	NR	.99	-	.043	.043	.043	NR
"	4/457	714	1.5	"	310/1000	"	"	1.44	.50	.042	.045	NR	1.36	-	.038	.070	.070	.070	NR	.99	-	.043	.043	.043	NR
"	5/458	1100	1.5	65°	310/1000	"	"	1.51	.50	.040	.045	NR	1.36	-	.038	.070	.070	.070	NR	.99	-	.043	.043	.043	NR
"	6/459	1117	1.5	"	"	"	"	1.17	.56	.050	.045	NR	1.94	-	.030	.070	.070	.070	NR	.61	-	.043	.043	.043	NR
"	7/460	1200	1.5	"	340/1000	"	"	1.44	.61	.051	.043	NR	1.15	-	.045	.070	.070	.070	NR	.61	-	.043	.043	.043	NR
"	8/461	1219	1.5	"	"	"	"	1.51	.61	.043	.049	NR	1.45	-	.044	.070	.070	.070	NR	.51	-	.043	.043	.043	NR
4-14-64	1/462	700	1.5	48°	300/15	"	"	1.15	-	.046	.070	NR	1.14	-	.042	.070	.070	.070	NR	.23	-	.040	.040	.040	NR
"	2/463	750	1.5	58°	310/15	"	"	.97	-	.041	.070	NR	1.21	-	.041	.070	.070	.070	NR	.23	-	.040	.040	.040	NR
"	3/464	859	1.5	"	"	"	"	1.01	.54	.050	.070	NR	1.21	-	.041	.070	.070	.070	NR	.23	-	.040	.040	.040	NR
"	4/465	919	1.5	65°	"	"	"	1.01	.54	.050	.070	NR	1.21	-	.041	.070	.070	.070	NR	.23	-	.040	.040	.040	NR
"	5/466	1100	1.5	65°	"	"	"	1.01	.54	.050	.070	NR	1.21	-	.041	.070	.070	.070	NR	.23	-	.040	.040	.040	NR
"	6/467	1130	1.5	"	"	"	"	1.12	.54	.045	.070	NR	1.21	-	.041	.070	.070	.070	NR	.23	-	.040	.040	.040	NR
"	7/468	1200	1.5	"	310/15	"	"	1.12	.54	.045	.070	NR	1.21	-	.041	.070	.070	.070	NR	.23	-	.040	.040	.040	NR
"	8/469	1219	1.5	"	"	"	"	1.23	-	.052	.070	NR	1.21	-	.041	.070	.070	.070	NR	.23	-	.040	.040	.040	NR
4-15-64	1/470	700	1.5	48°	120/15	"	"	.82	-	.047	.070	NR	1.21	-	.041	.070	.070	.070	NR	.23	-	.040	.040	.040	NR
"	2/471	719	1.5	50°	"	"	"	1.00	.54	.048	.070	NR	1.21	-	.041	.070	.070	.070	NR	.23	-	.040	.040	.040	NR
"	3/472	851	1.5	"	120/15	"	"	1.20	.54	.047	.070	NR	1.21	-	.041	.070	.070	.070	NR	.23	-	.040	.040	.040	NR
"	4/473	1200	1.5	"	"	"	"	1.20	.54	.047	.070	NR	1.21	-	.041	.070	.070	.070	NR	.23	-	.040	.040	.040	NR

Table VII.- Continued.

OPERATING CONDITIONS				WEATHER			SONIC BOOM PRESSURE SIGNATURE DATA												
Date	Flight No.	Time	Mach No.	Surface Temp.	Surface Winds	Cloud Cover	Precipitation	Station 1				Station 3				Station 4			
								ΔP_0	ΔP_1	ΔI_0 Pos	Wave Shape	ΔP_0	ΔP_1	ΔI_0 Pos	Wave Shape	ΔP_0	ΔP_1	ΔI_0 Pos	Wave Shape
4-2-64	1/15	12:05	1.5	72°	110/1235	⊕	None	1.13	-	-	NR	1.06	-	-	NR	0.419	0.043	0.013	NR
"	2/15	11:15	1.5	71°	150/1235	"	"	1.15	-	-	N	1.47	-	-	NR	0.413	0.047	0.011	NR
"	3/15	8:31	1.5	62°	420/10	⊕	"	1.22	-	-	NR	1.40	-	-	NR	0.427	0.043	0.012	NR
"	4/15	7:10	1.5	"	"	"	"	1.11	-	-	NR	1.41	-	-	NR	0.428	0.043	0.012	NR
"	5/15	11:05	1.5	70°	470/10	⊕	"	1.27	-	-	N	1.03	-	-	NR	0.435	0.045	0.011	NR
"	6/15	11:05	1.5	"	"	"	"	1.21	-	-	N	1.12	-	-	NR	0.428	0.045	0.011	NR
"	7/15	11:05	1.5	60°	100/10+15	⊕	"	1.28	-	-	NP	1.10	-	-	N	0.419	0.041	0.014	NR
"	8/15	11:05	1.5	"	"	"	"	1.42	-	-	NR	1.25	-	-	N	0.427	0.041	0.015	NR
4-2-64	1/15	12:00	1.5	72°	110/1235	⊕	"	1.13	-	-	N	1.17	-	-	NR	0.416	0.043	0.011	NR
"	2/15	11:15	1.5	"	"	"	"	1.13	-	-	N	1.24	-	-	NR	0.428	0.043	0.011	NR
"	3/15	11:15	1.5	76°	140/1235	⊕	"	1.13	-	-	N	1.20	-	-	NR	0.428	0.043	0.012	NR
"	4/15	11:15	1.5	"	"	"	"	1.44	-	-	NP	1.34	-	-	NR	0.427	0.043	0.013	NR
4-2-64	1/15	7:00	1.5	65°	110/1235	⊕	F	1.02	-	-	N	1.17	-	-	N	0.428	0.043	0.012	NR
"	2/15	7:00	1.5	"	"	⊕	"	1.51	-	-	NR	1.18	-	-	NR	0.428	0.043	0.012	NR
"	3/15	7:00	1.5	"	"	⊕	"	1.13	-	-	NR	1.07	-	-	NR	0.428	0.043	0.012	NR
"	4/15	7:17	1.5	"	"	"	"	1.13	-	-	NR	1.07	-	-	NR	0.428	0.043	0.012	NR
"	5/15	11:00	1.5	75°	150/1235	"	None	1.10	-	-	NR	1.07	-	-	R	0.428	0.043	0.012	NR
"	6/15	11:00	1.5	"	"	"	"	1.13	-	-	NR	1.07	-	-	NR	0.428	0.043	0.012	NR
"	7/15	12:00	1.5	80°	150/1235	⊕	"	1.11	-	-	NR	1.14	-	-	NR	0.428	0.043	0.012	NR
"	8/15	12:00	1.5	"	"	⊕	"	1.47	-	-	NP	1.05	-	-	NR	0.428	0.043	0.012	NR
4-2-64	1/15	7:00	1.5	68°	150/10	⊕	"	1.04	-	-	N	1.05	-	-	NR	0.428	0.043	0.012	NR
"	2/15	7:00	1.5	"	"	⊕	"	1.06	-	-	N	1.05	-	-	NR	0.428	0.043	0.012	NR
"	3/15	7:00	1.5	"	"	⊕	"	1.14	-	-	NR	1.05	-	-	N	0.428	0.043	0.012	NR
"	4/15	7:00	1.5	"	"	"	"	1.14	-	-	NR	1.05	-	-	N	0.428	0.043	0.012	NR
"	5/15	11:00	1.5	68°	150/15	"	"	1.14	-	-	NR	1.05	-	-	NR	0.428	0.043	0.012	NR
"	6/15	11:00	1.5	"	"	"	"	1.10	-	-	N	1.05	-	-	NR	0.428	0.043	0.012	NR
"	7/15	12:00	1.5	70°	150/10	⊕	"	1.11	-	-	N	1.05	-	-	N	0.428	0.043	0.012	NR
"	8/15	12:00	1.5	"	"	⊕	"	1.11	-	-	N	1.05	-	-	N	0.428	0.043	0.012	NR
4-2-64	1/15	7:00	1.5	60°	150/15	⊕	"	1.04	-	-	N	1.05	-	-	N	0.428	0.043	0.012	NR
"	2/15	7:00	1.5	"	"	⊕	"	1.04	-	-	N	1.05	-	-	N	0.428	0.043	0.012	NR
"	3/15	7:00	1.5	61°	150/15+00	"	"	1.04	-	-	N	1.05	-	-	N	0.428	0.043	0.012	NR
"	4/15	11:00	1.5	"	"	"	"	1.04	-	-	N	1.05	-	-	N	0.428	0.043	0.012	NR
"	5/15	11:00	1.5	"	"	"	"	1.04	-	-	N	1.05	-	-	N	0.428	0.043	0.012	NR
"	6/15	11:00	1.5	"	"	"	"	1.04	-	-	N	1.05	-	-	N	0.428	0.043	0.012	NR

Table VII.- Concluded.

OPERATING CONDITIONS				WEATHER				SONIC BOOM PRESSURE SIGNATURE DATA														
Date	Flight No.	Time	Mach No.	Surface Temp.	Surface Winds	Cloud Cover	Precipitation	Station 1					Station 3					Station 4				
								ΔP_0	ΔP_1	ΔI_0 Pos	I_0 Pos	Wave Shape	ΔP_0	ΔP_1	ΔI_0 Pos	I_0 Pos	Wave Shape	ΔP_0	ΔP_1	ΔI_0 Pos	I_0 Pos	Wave Shape
4-1-64	1/54	889	1.5	68°	190/10+5	⊕	None	1.36	-	0.043	0.0500	N	1.09	-	0.044	0.0551	NR	0.54	-	0.050	0.0153	NR
"	2/54	720	1.5	"	"	"	"	1.20	-	0.041	0.0503	NR	1.25	-	0.039	0.0523	NR	.77	-	0.056	0.012	NR
"	3/54	1059	1.5	"	110/20	"	"	.68	-	0.050	0.0500	NR	.76	-	0.08	0.0194	NR	.34	-	0.060	0.0130	NR
"	4/54	1119	1.5	"	"	"	"	.48	-	0.054	0.056	NR	.91	-	0.065	0.0423	NR	.51	-	0.082	0.0165	NR
4-1-64	1/54	615	1.5	58°	200/10	⊕	"	1.25	-	0.045	0.049	NR	.45	-	0.045	0.0522	NR	1.56	-	0.048	0.0177	-
"	2/54	713	1.5	"	"	"	"	1.25	-	0.049	0.0515	NR	1.62	-	0.046	0.0529	NR	.77	-	0.056	0.0126	NR
"	3/54	720	1.5	66°	110/15+5	"	"	1.43	-	0.044	0.0560	NR	1.47	-	0.046	0.0523	NR	.79	-	0.051	0.011	NR
"	4/54	117	1.5	"	"	"	"	.55	-	0.051	0.056	NR	1.59	-	0.047	0.0527	NR	1.44	-	0.045	0.015	NR
"	5/54	1059	1.5	69°	200/10+5	⊕	"	1.09	-	0.049	0.056	NR	.64	-	0.055	0.060	NR	.66	-	0.063	0.0114	NR
"	6/54	1119	1.5	"	"	"	"	1.20	-	0.043	0.049	NR	1.10	-	0.052	0.0581	NR	.75	-	0.053	0.012	NR
"	7/54	1220	1.5	72°	"	⊕	"	1.47	-	0.050	0.059	NR	1.07	-	0.054	0.0554	NR	.52	-	0.050	0.0123	NR
"	8/54	1220	1.5	"	"	"	"	.97	-	0.046	0.0561	NR	.72	-	0.045	0.0581	NR	.94	-	0.084	0.0157	NR
4-1-64	1/54	700	1.5	54°	210/15+20	⊕	"	1.29	-	0.045	0.045	NR	1.23	-	0.051	0.0558	NR	1.56	-	0.054	0.0412	NR
"	2/54	117	1.5	"	"	"	"	1.35	-	0.048	0.046	NR	1.61	-	0.050	0.0497	NR	1.67	-	0.051	0.0288	NR
"	3/54	889	1.5	60°	210/10+20	⊕	"	.75	-	0.059	0.049	NR	1.79	-	0.048	0.0622	NR	1.25	-	0.054	0.014	NR
"	4/54	720	1.5	"	"	"	"	1.81	-	0.051	0.0544	NR	1.64	-	0.052	0.0566	NR	1.33	-	0.051	0.024	NR
"	5/54	1120	1.5	62°	"	⊕	"	.72	-	0.052	0.051	NR	.80	-	0.055	0.0496	NR	1.26	-	0.052	0.022	NR
"	6/54	1120	1.5	"	"	"	"	1.29	-	0.043	0.0497	NR	1.61	-	0.041	0.0546	NR	1.77	-	0.044	0.044	NR
"	7/54	1220	1.5	63°	"	⊕	"	1.01	-	0.047	0.054	NR	1.24	-	0.047	0.0505	NR	1.50	-	0.045	0.026	NR
"	8/54	1220	1.5	"	"	"	"	.72	-	0.048	0.0477	NR	1.13	-	0.055	0.0550	NR	1.58	-	0.045	0.022	NR
4-1-64	5/54	1120	1.5	64°	060/10	⊕	"	1.00	-	0.044	0.0561	P	1.24	-	0.047	0.0584	P	1.03	-	0.050	0.0270	P
"	6/54	1120	1.5	"	"	"	"	1.56	-	0.045	0.0577	P	1.69	-	0.050	0.0585	NR	1.29	-	0.054	0.014	P
4-1-64	1/54	629	1.5	52°	140/10	⊕	"	1.04	-	0.045	0.064	NR	1.53	-	0.040	0.061	NR	.72	-	0.058	0.0122	NR
"	2/54	713	1.5	"	"	"	"	.68	-	0.045	0.0523	NR	1.18	-	0.036	0.0526	NR	.68	-	0.055	0.013	NR
"	3/54	889	1.5	65°	180/10	"	"	.68	-	0.047	0.0493	NR	1.30	-	0.041	0.0526	NR	1.57	-	0.058	0.0122	NR
"	4/54	713	1.5	"	"	"	"	.68	-	0.047	0.054	NR	1.26	-	0.045	0.054	NR	.85	-	0.050	0.0179	NR
"	5/54	1059	1.5	70°	"	"	RW	1.00	-	0.045	0.057	NR	1.26	-	0.047	0.0501	NR	1.14	-	0.050	0.012	NR
"	6/54	1120	1.5	"	"	"	"	.71	-	0.057	0.055	NR	1.21	-	0.046	0.0501	NR	1.48	-	0.054	0.017	NR
"	7/54	1220	1.5	73°	"	"	"	.60	-	0.052	0.057	NR	1.05	-	0.052	0.055	NR	1.57	-	0.050	0.021	NR
"	8/54	1219	1.5	"	"	"	"	1.22	-	0.040	0.0546	NR	1.07	-	0.040	0.0562	NR	1.43	-	0.056	0.0200	NR
5-1-64	4/54	111	1.5	62°	160/10+5	⊕	"	1.00	-	0.045	0.041	NR	1.57	-	0.042	0.0594	P	1.06	-	0.050	0.028	NR

Table VIII.- Summary Of Sonic Boom Data For Various Flights Of Airplane A For An
Altitude Range Of 26,000 To 27,000 Feet

OPERATING CONDITIONS				WEATHER				SONIC BOOM PRESSURE SIGNATURE DATA														
Date	Flight No.	Time	Mach No.	Surface Temp.	Surface Winds	Cloud Cover	Precipitation	Station 1					Station 3					Station 4				
								ΔP_0	ΔP_I	ΔI_0 Pos.	I_0 Pos.	Wave Shape	ΔP_0	ΔP_I	ΔI_0 Pos.	I_0 Pos.	Wave Shape	ΔP_0	ΔP_I	ΔI_0 Pos.	I_0 Pos.	Wave Shape
27,000 FT.																						
2-11-64	7/564	700	1.7	57°	170/E	⊕	Clear	1.44	0.51	0.025	0.0717	N	1.61	0.50	0.041	0.0232	N	1.18	0.32	0.044	0.015	N
"	7/564	1100	1.5	65°	120/10	"	"	1.59	.66	.030	0.0315	NP	1.74	.47	.052	0.0271	NP	.67	.28	.062	.0151	"
"	7/564	1100	1.5	"	"	"	"	1.46	.68	.039	0.0255	NP	1.31	.49	.041	0.0277	NP	.90	.28	.052	.0207	"
"	7/564	1200	1.5	"	170/10	"	"	.98	.86	.040	0.0205	R	1.50	.48	.045	0.0232	NP	1.21	.30	.040	.0205	"
"	7/564	1300	1.7	"	"	"	"	1.10	.45	.046	0.0171	P	1.58	.47	.048	0.0263	NP	1.51	.36	.044	.0206	"
2-11-64	1/564	700	1.7	49°	220/10+25	⊕	"	.58	.21	.041	0.0156	R	1.18	.24	.051	0.0173	"	.17	.06	.043	.0037	"
"	1/564	700	1.7	"	"	"	"	.96	.35	.043	0.0197	R	1.51	.42	.027	0.0238	NP	.93	.22	.041	.0155	"
"	3/571	900	1.7	30°	250/10+25	⊕	S	.98	.30	.042	0.018	NR	1.37	.33	.028	0.0181	NP	1.27	.26	.040	.0207	"
"	5/573	1059	1.5	32°	220/15+40	"	"	1.52	.40	.040	0.014	NP	1.10	.35	.042	0.0237	NP	.40	.16	.064	.0160	"
"	6/574	1100	1.5	"	"	"	"	.91	.40	.044	0.0184	NR	1.48	.34	.039	0.0211	N	.91	.20	.056	.0188	"
2-11-64	1/575	659	1.5	24°	260/10	○	Clear	1.22	.50	.046	0.026	NR	1.17	.39	.042	0.0267	NR	.70	.26	.052	.0171	"
"	4/576	859	1.5	26°	"	"	"	1.20	.44	.041	0.027	NR	1.23	.43	.043	0.0203	"	.78	.28	.046	.0197	"
"	4/578	1100	1.5	32°	"	"	"	1.15	.42	.047	0.0277	NR	.90	.36	.041	0.0218	R	.57	.25	.057	.0188	"
2-11-64	2/575	900	1.3	75°	180/15+20	"	"	.93	-	.053	0.0239	R	1.00	-	.036	0.0187	"	.64	-	.061	.0175	"
"	4/576	900	1.3	"	"	"	"	.96	-	.057	0.0240	R	.69	-	.052	0.0167	"	.42	-	.060	.0175	"
"	5/577	1100	1.3	80°	190/15+25	"	"	1.63	-	.046	0.0250	NP	.48	-	.059	0.0189	"	.74	-	.066	.0200	"
"	6/578	1100	1.3	"	"	"	"	1.26	-	.065	0.0242	R	-	-	-	-	"	-	-	-	-	"
"	7/577	1300	1.3	84°	"	"	"	.93	-	.050	0.0202	R	1.63	-	.050	0.0261	NP	1.37	-	.059	.0207	"
26,000 FT.																						
2-11-64	2/577	900	1.5	32°	260/10	○	"	1.10	0.44	0.043	0.0233	NR	1.42	0.43	0.045	0.0229	N	0.65	0.28	0.048	0.0184	N
"	5/578	1100	1.5	"	"	"	"	1.25	.44	.045	0.0238	NR	.92	.31	.041	0.0226	R	.43	.22	.056	.0162	"

Table IX.- Summary Of Sonic Boom Data For Various Flights Of Airplane A
For An Altitude Of 24,000 Feet

OPERATING CONDITIONS				WEATHER				SONIC BOOM PRESSURE SIGNATURE DATA														
Date	Flight No.	Time	Mach No.	Surface Temp.	Surface Winds	Cloud Cover	Precipitation	Station 1					Station 3					Station 4				
								ΔP_0	ΔP_1	ΔI_0 Pos	I_0 Pos	Wave Shape	ΔP_0	ΔP_1	ΔI_0 Pos	I_0 Pos	Wave Shape	ΔP_0	ΔP_1	ΔI_0 Pos	I_0 Pos	Wave Shape
1-25-64	1/25	700	1.5	58°	150/10	⊙	FW	1.41	-	0.046	0.0166	N	1.40	-	0.046	0.0151	N	0.66	-	0.055	0.0160	N
"	1/25	710	1.5	"	"	"	"	.95	-	.047	0.051	N	1.66	-	.053	0.047	"	.77	-	.049	.051	N
"	1/25	720	1.5	57°	100/10+15	⊕	"	1.16	-	.046	0.0230	N	1.77	-	.046	0.011	N	.64	-	0.05	0.025	"
1-25-64	1/25	700	1.5	60°	160/15+20	⊙	None	1.49	-	.051	0.047	N	.59	-	.055	0.002	N	.34	-	.178	0.010	N
"	1/25	717	1.4	"	"	"	"	1.66	-	.047	0.055	N	1.19	-	.045	0.013	N	1.01	-	.050	0.060	N
1-25-64	1/25	700	1.4	60°	170/10+20	⊙	"	1.77	-	.048	0.011	N	.90	-	.055	0.027	N	.65	-	.051	0.010	N
"	1/25	710	1.4	"	"	"	"	1.71	-	.020	0.015	NP	1.20	-	.049	0.010	N	.47	-	.050	0.010	N
"	1/25	809	1.4	75°	170/15+20	⊕	"	.97	-	.051	0.023	N	1.03	-	.046	0.027	N	.60	-	0.010	0.010	N
"	1/25	930	1.5	"	"	"	"	1.60	-	.041	0.064	NP	1.14	-	.057	0.017	N	.67	-	0.010	0.010	N
"	1/25	1100	1.4	70°	150/15+25	"	"	1.73	-	.041	0.093	N	1.16	-	.041	0.051	N	.69	-	0.010	0.010	N
"	1/25	1120	1.5	"	"	"	"	1.13	-	.050	0.064	N	1.30	-	.045	0.057	N	.78	-	0.010	0.010	N
"	1/25	1200	1.4	80°	"	"	"	.88	-	.052	0.040	N	.75	-	.057	0.027	N	.60	-	0.010	0.010	N
"	1/25	1219	1.4	"	"	"	"	.95	-	.048	0.037	N	1.55	-	.040	0.066	N	.70	-	0.010	0.010	N
1-25-64	1/25	700	1.4	68°	170/15+25	"	"	1.94	-	.044	0.026	NP	1.01	-	.051	0.017	N	-	-	-	-	-
"	1/25	720	1.5	"	"	"	"	.65	-	.051	0.0195	"	1.30	-	.040	0.028	N	.64	-	.057	0.010	N
"	1/25	740	1.5	73°	"	"	"	1.50	-	.046	0.054	N	1.56	-	.058	0.050	N	.99	-	.050	0.010	N
"	1/25	750	1.5	"	"	"	"	.97	-	.057	0.066	N	.71	-	.055	0.010	N	1.10	-	.046	0.010	N
"	1/25	1100	1.5	70°	170/20+30	"	"	1.19	-	.049	0.080	N	1.40	-	.050	0.050	N	.91	-	.046	0.010	N
"	1/25	1120	1.5	"	"	"	"	.67	-	.051	0.053	N	.90	-	.050	0.050	N	.40	-	.050	0.010	N
"	1/25	1258	1.5	75°	"	⊕	"	1.60	-	.050	0.070	NP	.99	-	.050	0.049	N	.68	-	.050	0.010	N

Table X.- Summary Of Sonic Boom Data For Various Flights Of Airplane A For An
Altitude Range Of 21,000 To 23,000 Feet

[illegible]

Table XI.- Summary Of Sonic Boom Data For Various Flights Of Airplane B
For An Altitude Of 46,000 Feet

OPERATING CONDITIONS				WEATHER				SONIC BOOM PRESSURE SIGNATURE DATA															
Date	Flight No.	Time	Mach No.	Surface Temp.	Surface Winds	Cloud Cover	Precipitation	Station 1					Station 3					Station 4					Wave Shape
								ΔP_0	ΔP_1	Δt_0 Pos	I_0 Pos	Wave Shape	ΔP_0	ΔP_1	Δt_0 Pos	I_0 Pos	Wave Shape	ΔP_0	ΔP_1	Δt_0 Pos	I_0 Pos	Wave Shape	
5/1/64	1/705	700	1.4	60°	170/10	①	F	.029	-	.0287	.0444	NR	1.05	-	.0281	.0435	NR	1.41	-	.0287	.0444	NR	Z
"	2/706	717	1.4	"	"	"	"	1.10	-	.0287	.0437	NR	1.10	-	.0287	.0437	NR	1.41	-	.0287	.0437	NR	Z
"	3/706	900	1.4	75°	"	"	None	1.58	-	.0287	.0437	NR	.84	-	.111	.0604	NR	.74	-	.105	.0437	NR	Z
"	4/707	917	1.4	"	"	"	"	-	-	-	-	-	1.75	-	.072	.0600	NR	1.84	-	.072	.0600	NR	Z
"	5/707	1101	1.4	70°	200/15	②	"	1.00	-	.090	.0386	NR	1.54	-	.072	.0598	NR	1.84	-	.072	.0598	NR	Z
"	6/707	1121	1.4	"	"	"	"	.84	-	.0287	.0411	NR	1.74	-	.050	.0599	NR	.95	-	.104	.0437	NR	Z
"	7/707	1300	1.4	25°	210/10+15	"	"	1.44	-	.0287	.0440	NR	1.41	-	.051	.0590	NR	.81	-	.010	.0437	NR	Z
"	8/707	1314	1.4	"	"	"	"	.94	-	.0287	.0435	NR	.79	-	.058	.0420	NR	1.81	-	.027	.0437	NR	Z
5/2/64	1/707	701	1.5	60°	120/10	①	"	1.09	-	.0287	.0414	NR	1.11	-	.066	.0430	NR	.93	-	.074	.0437	NR	Z
"	2/707	715	1.5	"	"	"	"	1.07	-	.0287	.0407	NR	1.04	-	.054	.0434	NR	1.13	-	.071	.0437	NR	Z
"	3/707	855	1.5	77°	"	"	"	1.11	-	.072	.0437	NR	1.71	-	.067	.0544	NR	1.54	-	.071	.0437	NR	Z
"	4/707	917	1.5	"	"	"	"	1.16	-	.071	.0436	NR	1.18	-	.065	.0433	NR	1.42	-	.076	.0437	NR	Z
"	5/710	1059	1.5	85°	210/10	"	"	1.00	-	.0287	.0433	NR	1.40	-	.076	.0523	NR	1.41	-	.076	.0523	NR	Z
"	6/711	1120	1.5	"	"	"	"	.89	-	.090	.0384	NR	1.71	-	.074	.0507	NR	1.36	-	.072	.0507	NR	Z
"	7/712	1200	1.5	25°	180/10	"	"	.96	-	.0287	.0433	NR	1.14	-	.054	.0436	NR	1.40	-	.077	.0437	NR	Z
"	8/712	1324	1.5	"	"	"	"	1.24	-	.0287	.0437	NR	.67	-	.076	.0331	NR	.71	-	.083	.0437	NR	Z
5/3/64	1/714	700	1.5	67°	180/10	②	"	1.27	-	.0287	.0545	NR	1.45	-	.076	.0554	NR	1.46	-	.085	.0437	NR	Z
"	2/715	717	1.5	"	"	"	"	1.36	-	.079	.0581	NR	1.41	-	.070	.0457	NR	1.31	-	.073	.0437	NR	Z
"	3/716	900	1.5	75°	"	"	"	1.24	-	.090	.0511	NR	1.41	-	.071	.0515	NR	1.31	-	.076	.0437	NR	Z
"	4/717	921	1.5	"	"	"	"	1.01	-	.078	.0433	NR	1.58	-	.073	.0451	NR	1.06	-	.078	.0437	NR	Z
"	5/718	1101	1.5	71°	"	"	"	1.01	-	.106	.0545	NR	1.53	-	.094	.0560	NR	1.11	-	.091	.0437	NR	Z
"	6/719	1121	1.5	"	"	"	"	1.24	-	.081	.0547	NR	1.57	-	.065	.0519	NR	.50	-	.113	.0437	NR	Z
"	7/720	1300	1.5	25°	190/10+20	"	"	1.03	-	.094	.0584	NR	.77	-	.103	.0464	NR	.59	-	.095	.0437	NR	Z
"	8/721	1324	1.5	"	"	"	"	1.24	-	.0287	.0507	NR	1.37	-	.091	.0461	NR	1.42	-	.083	.0437	NR	Z
5/4/64	1/722	609	1.5	68°	180/10	①	"	1.28	-	.080	.0585	NR	1.24	-	.070	.0512	NR	1.44	-	.093	.0437	NR	Z
"	2/723	717	1.5	"	"	"	"	.98	-	.098	.0453	NR	.38	-	.078	.0434	NR	.81	-	.085	.0437	NR	Z
5/5/64	1/726	1200	1.5	25°	120/10+20	"	"	1.41	-	.077	.0594	NR	1.18	-	.076	.0473	NR	.70	-	.087	.0437	NR	Z
"	2/727	1300	1.5	"	"	"	"	.93	-	1.00	.0500	NR	.16	-	.101	.0407	NR	1.19	-	.086	.0437	NR	Z
5/6/64	5/727	1315	1.5	52°	130/10+15	④	"	1.26	-	.082	.0510	NR	1.10	-	.072	.0442	NR	.55	-	.100	.0437	NR	K

Table XII.- Summary Of Sonic Boom Data For Various Flights Of Airplane B
For An Altitude Of 44,000 Feet

OPERATING CONDITIONS				WEATHER				SONIC BOOM PRESSURE SIGNATURE DATA														
Date	Flight No.	Time	Mach No.	Surface Temp.	Surface Winds	Cloud Cover	Precipitation	Station 1					Station 3					Station 4				
								ΔP_0	ΔP_1	Δt_0 Pos	I_0 Pos	Wave Shape	ΔP_0	ΔP_1	Δt_0 Pos	I_0 Pos	Wave Shape	ΔP_0	ΔP_1	Δt_0 Pos	I_0 Pos	Wave Shape
Series 1	3/74	700	1.5	70	140/15+20	①	None	1.79	-	0.084	0.0596	N P	1.11	-	0.081	0.0524	N P	0.81	-	0.073	0.0414	N P
"	4/74	700	1.5	"	"	"	"	1.18	-	0.078	0.0589	N P	1.31	-	0.071	0.0514	N P	1.05	-	0.073	0.0414	N P
"	5/74	1058	1.5	81°	"	②	"	1.37	-	0.082	0.0587	N P	1.13	-	0.071	0.0601	N P	1.03	-	0.073	0.0414	N P
"	6/74	1118	1.5	"	"	"	"	1.50	-	0.079	0.0565	N P	1.48	-	0.081	0.0451	N P	1.19	-	0.076	0.0475	N P
"	7/74	1200	1.5	83°	"	"	"	1.45	-	0.080	0.0601	N P	1.16	-	0.073	0.0624	N P	1.24	-	0.076	0.0475	N P
"	8/74	1220	1.5	"	"	"	"	1.28	-	0.093	0.0421	N P	1.47	-	0.076	0.0517	N P	1.54	-	0.074	0.0420	N P
Series 2	1/74	700	1.5	69°	150/15+20	①	"	-	-	-	-	-	1.57	-	0.072	0.0422	N P	1.91	-	0.071	0.0442	N P
"	2/74	701	1.5	"	"	"	"	1.20	-	0.075	0.0518	N P	1.49	-	0.071	0.0517	N P	1.94	-	0.082	0.0421	N P
"	3/74	859	1.5	72°	190/10+20	②	"	1.20	-	0.081	0.0635	N P	1.38	-	0.074	0.0426	N P	1.86	-	0.080	0.0421	N P
"	4/74	913	1.5	"	"	"	"	1.76	-	0.069	0.0587	N P	1.58	-	0.074	0.0487	N P	1.84	-	0.075	0.0421	N P
"	5/74	1000	1.5	79°	150/10+20	①	"	1.51	-	0.085	0.0630	N P	1.76	-	0.070	0.0556	N P	1.88	-	0.073	0.0421	N P
"	6/74	1121	1.5	"	"	"	"	1.24	-	0.082	0.0578	N P	1.60	-	0.067	0.0451	N P	1.81	-	0.076	0.0462	N P
Series 3	1/74	659	1.5	72°	180/15+20	"	"	1.57	-	0.072	0.0507	N P	1.32	-	0.068	0.0491	N P	1.54	-	0.071	0.0442	N P
"	2/74	700	1.5	"	"	"	"	1.12	-	0.071	0.0417	N P	1.32	-	0.071	0.0459	N P	1.74	-	0.077	0.0474	N P
"	3/74	703	1.5	78°	170/10	"	"	1.22	-	0.074	0.0423	N P	1.47	-	0.067	0.0463	N P	1.44	-	0.076	0.0474	N P
"	4/74	1100	1.5	76°	"	③	"	1.11	-	0.078	0.0500	N P	1.72	-	0.085	0.0445	N P	1.15	-	0.077	0.0423	N P
"	5/74	1300	1.5	88°	"	"	"	1.63	-	0.069	0.0455	N P	1.57	-	0.075	0.0460	N P	1.86	-	0.074	0.0470	N P
"	6/74	1220	1.5	"	"	"	"	1.16	-	0.079	0.0414	N P	1.51	-	0.069	0.0494	N P	1.54	-	0.078	0.0470	N P
Series 4	1/74	659	1.5	75°	"	④	"	1.22	-	0.084	0.0544	N P	1.28	-	0.084	0.0568	N P	1.80	-	0.092	0.0420	N P
"	2/74	701	1.5	"	"	"	"	1.17	-	0.070	0.0397	N P	1.32	-	0.072	0.0460	N P	1.79	-	0.086	0.0471	N P
"	3/74	859	1.5	74°	190/10	"	"	1.57	-	0.073	0.0506	N P	1.96	-	0.077	0.0417	N P	1.65	-	0.075	0.0420	N P
"	4/74	1058	1.5	88°	150/10	"	"	1.14	-	0.067	0.0495	N P	1.47	-	0.067	0.0419	N P	1.57	-	0.078	0.0420	N P
"	5/74	1113	1.5	"	"	"	"	1.22	-	0.065	0.0441	N P	1.10	-	0.061	0.0420	N P	1.91	-	0.080	0.0409	N P
"	6/74	1300	1.5	92°	170/10	"	"	1.22	-	0.070	0.0478	N P	1.05	-	0.072	0.0584	N P	1.88	-	0.073	0.0421	N P
"	7/74	1221	1.5	"	"	"	"	1.26	-	0.076	0.0366	N P	1.16	-	0.080	0.0611	N P	1.40	-	0.079	0.0421	N P
Series 5	1/74	659	1.5	72°	170/10	⑤	"	1.20	-	0.078	0.0401	N P	1.10	-	0.076	0.0470	N P	1.80	-	0.079	0.0420	N P
"	2/74	701	1.5	"	"	"	"	1.12	-	0.068	0.0384	N P	1.32	-	0.067	0.0417	N P	1.74	-	0.087	0.0474	N P
"	3/74	859	1.5	78°	180/10	"	"	1.22	-	0.074	0.0423	N P	1.71	-	0.070	0.0417	N P	1.45	-	0.082	0.0473	N P
"	4/74	1100	1.5	76°	170/10	"	"	1.11	-	0.078	0.0500	N P	1.57	-	0.075	0.0460	N P	1.86	-	0.074	0.0470	N P
"	5/74	1300	1.5	88°	"	"	"	1.22	-	0.070	0.0478	N P	1.10	-	0.072	0.0584	N P	1.88	-	0.073	0.0421	N P
"	6/74	1221	1.5	"	"	"	"	1.26	-	0.076	0.0366	N P	1.16	-	0.080	0.0611	N P	1.40	-	0.079	0.0421	N P

Table XII.- Concluded.

OPERATING CONDITIONS				WEATHER				SONIC BOOM PRESSURE SIGNATURE DATA														
Date	Flight No.	Time	Mach No.	Surface Temp.	Surface Winds	Cloud Cover	Precipitation	Station 1					Station 3					Station 4				
								ΔP_0	ΔP_1	Δt_0 Pos	I_0 Pos	Wave Shape	ΔP_0	ΔP_1	Δt_0 Pos	I_0 Pos	Wave Shape	ΔP_0	ΔP_1	Δt_0 Pos	I_0 Pos	Wave Shape
5-1-64	1/760	658	1.5	70°	12/10+15	⊙	None	1.38	-	0.015	0.041	N	1.06	-	0.025	0.046	NR	1.32	-	0.013	0.045	N
	2/761	700	1.5	"	"	"	"	1.02	-	0.016	0.040	NR	1.21	-	0.024	0.045	T	1.15	-	0.025	0.044	N
	3/762	839	1.5	71°	19/10+15	"	"	.75	-	.084	0.040	NR	1.21	-	.076	0.045	NP	1.12	-	.075	0.041	N
	4/763	1057	1.5	"	"	⊙	TRW	1.24	-	.085	0.046	NR	1.19	-	.087	0.051	R	.97	-	.084	0.040	N
	5/764	1119	1.5	"	"	"	"	1.17	-	.090	0.040	NR	1.15	-	.073	0.052	R	1.21	-	.081	0.041	N
5-5-64	1/765	1258	1.5	74°	"	"	"	1.14	-	.078	0.045	NR	1.23	-	.072	0.048	R	1.25	-	.072	0.043	N
	2/766	658	1.5	56°	360/15	"	None	.77	-	.091	0.037	NR	1.21	-	.065	0.044	NR	.78	-	.073	0.047	N
	3/767	721	1.5	"	"	"	"	1.16	-	.081	0.057	NR	.52	-	.076	0.047	NR	.68	-	.100	0.040	"
	4/770	839	1.5	"	"	"	"	1.30	-	.072	0.032	N	1.25	-	.070	0.041	N	.90	-	.074	0.040	N
	5/771	1059	1.5	59°	"	"	"	.90	-	.070	0.041	NR	1.06	-	.076	0.042	NR	.77	-	.086	0.040	N
5-9-64	1/772	1119	1.5	"	"	"	"	1.01	-	.072	0.042	NR	.81	-	.087	0.041	NR	1.75	-	.070	0.045	"
	2/773	1258	1.5	62°	"	"	"	1.12	-	.079	0.040	NR	1.71	-	.065	0.041	NP	2.02	-	.069	0.040	"
	3/774	700	1.5	59°	040/10	"	TRW	.72	-	.173	0.049	"	.49	-	.094	0.041	T	.76	-	.120	0.077	"
	4/775	719	1.5	"	"	"	"	.63	-	.100	0.051	C	.56	-	.166	0.041	T	.42	-	.076	0.074	"
	5/776	900	1.5	55°	"	"	"	.49	-	.090	0.040	R	.47	-	.114	0.041	T	.56	-	.116	0.076	"
5-11-64	1/777	700	1.5	"	"	"	"	.33	-	.098	0.049	"	.70	-	.075	0.041	N	.19	-	.158	0.015	"
	2/778	1200	1.5	58°	VAR/5	"	"	1.80	-	.085	0.052	C	1.53	-	.069	0.047	NP	.66	-	.094	0.044	"
	3/779	700	1.5	65°	050/10	⊙	None	.46	-	.100	0.049	R	1.10	-	.052	0.057	NR	.66	-	.098	0.046	"
	4/780	1200	1.5	"	"	⊙	"	.45	-	.069	0.055	NR	1.02	-	.054	0.057	NR	.33	-	.104	0.040	"
	5/781	700	1.5	53°	360/10	⊙	RWF	1.37	-	.076	0.057	NR	1.55	-	.066	0.051	N	1.14	-	.078	0.045	N
5-21-64	1/782	700	1.5	"	"	"	"	1.11	-	.072	0.041	NR	1.24	-	.077	0.042	N	1.24	-	.086	0.048	N
	2/783	700	1.5	"	070/10	"	"	1.44	-	.087	0.056	N	1.21	-	.073	0.046	NP	1.24	-	.079	0.056	N
	3/784	900	1.5	"	"	"	RW	1.01	-	.090	0.047	NR	1.29	-	.068	0.053	NP	1.16	-	.065	0.055	"
	4/785	1057	1.5	56°	020/10	"	"	1.53	-	.072	0.042	NR	1.24	-	.077	0.048	N	1.10	-	.060	0.041	T
	5/786	1201	1.5	66°	070/15	"	None	1.16	-	.082	0.042	NR	1.24	-	.075	0.042	NP	.61	-	.115	0.052	"
	6/787	1201	1.5	"	"	"	"	1.48	-	.094	0.045	NR	1.27	-	.070	0.042	NR	.76	-	.106	0.043	"
	7/788	1201	1.5	"	"	"	"															"

Table XIII.- Summary of Sonic Boom Data For Various Flights Of Airplane B For An
Altitude Range of 33,000 To 42,000 Feet

OPERATING CONDITIONS				WEATHER				SONIC BOOM PRESSURE SIGNATURE DATA														
Date	Flight No.	Time	Mach No.	Surface Temp.	Surface Winds	Cloud Cover	Precipitation	Station 1					Station 3					Station 4				
								ΔP_0	ΔP_1	Δt_0 Pos.	I_0 Pos.	Wave Shape	ΔP_0	ΔP_1	Δt_0 Pos.	I_0 Pos.	Wave Shape	ΔP_0	ΔP_1	Δt_0 Pos.	I_0 Pos.	Wave Shape
42,000 FT.																						
5-15-64	7/674	11:20	1.4	62°	170/15	0	None	0.46	-	0.057	0.0400	NR	0.46	-	0.043	0.0487	-	0.00	-	0.00	-	-
"	7/675	11:25	1.4	"	"	"	"	0.46	-	0.057	0.0474	NR	1.34	-	0.057	0.0531	NR	2.64	-	0.00	-	-
"	7/676	11:30	1.4	"	170/15	0	"	1.39	-	0.057	0.0581	NR	1.34	-	0.057	0.0531	NR	2.64	-	0.00	-	-
"	7/677	11:35	1.4	"	"	"	"	1.01	-	0.057	0.0476	NR	1.34	-	0.057	0.0531	NR	2.64	-	0.00	-	-
"	7/678	11:40	1.4	57°	170/15	0	LWF	1.16	-	0.057	0.0476	NR	1.34	-	0.057	0.0531	NR	2.64	-	0.00	-	-
"	7/679	11:45	1.4	62°	170/15	0	None	1.04	-	0.057	0.0476	NR	1.34	-	0.057	0.0531	NR	2.64	-	0.00	-	-
"	7/680	11:50	1.4	"	"	"	"	0.76	-	0.057	0.0476	NR	1.34	-	0.057	0.0531	NR	2.64	-	0.00	-	-
40,000 FT.																						
5-15-64	7/681	12:00	1.4	74°	200/10	0	None	1.64	-	0.071	0.0547	NR	1.73	-	0.070	0.0637	NR	2.12	-	0.00	-	-
"	7/682	12:05	1.4	75°	170/15	"	"	1.67	-	0.070	0.063	NR	1.76	-	0.070	0.063	NR	2.12	-	0.00	-	-
"	7/683	12:10	1.4	"	"	"	"	1.17	-	0.070	0.0478	NR	1.76	-	0.070	0.063	NR	2.12	-	0.00	-	-
38,000 FT.																						
5-15-64	7/684	12:15	1.4	76°	180/15	0	None	1.43	-	0.079	0.0487	NR	1.53	-	0.082	-	NR	1.50	-	0.00	-	-
"	7/685	12:20	1.4	"	180/15	"	"	1.44	-	0.079	0.0492	NR	1.54	-	0.081	-	NR	1.50	-	0.00	-	-
"	7/686	12:25	1.4	"	"	"	"	1.01	-	0.079	0.0406	NR	1.54	-	0.081	-	NR	1.50	-	0.00	-	-
"	7/687	12:30	1.4	70°	200/15	0	"	1.43	-	0.079	0.0477	NR	1.56	-	0.081	0.0461	NR	1.50	-	0.00	-	-
"	7/688	12:35	1.4	"	"	"	"	1.00	-	0.079	0.0477	NR	1.56	-	0.081	0.0461	NR	1.50	-	0.00	-	-
"	7/689	12:40	1.4	65°	170/15	0	"	1.44	-	0.079	0.0461	NR	1.56	-	0.081	0.0461	NR	1.50	-	0.00	-	-
"	7/690	12:45	1.4	"	"	"	"	1.43	-	0.079	0.0459	NR	1.56	-	0.081	0.0461	NR	1.50	-	0.00	-	-
"	7/691	12:50	1.4	70°	"	0	"	1.43	-	0.079	0.0444	NR	1.60	-	0.083	0.0521	NR	1.50	-	0.00	-	-
"	7/692	12:55	1.4	"	"	"	"	1.43	-	0.079	0.0444	NR	1.60	-	0.083	0.0521	NR	1.50	-	0.00	-	-
"	7/693	13:00	1.4	75°	170/15	"	"	1.43	-	0.079	0.0444	NR	1.60	-	0.083	0.0521	NR	1.50	-	0.00	-	-
"	7/694	13:05	1.4	"	"	"	"	1.43	-	0.079	0.0444	NR	1.60	-	0.083	0.0521	NR	1.50	-	0.00	-	-
"	7/695	13:10	1.4	62°	170/15	"	"	1.43	-	0.079	0.0444	NR	1.60	-	0.083	0.0521	NR	1.50	-	0.00	-	-
"	7/696	13:15	1.4	"	"	"	"	1.43	-	0.079	0.0444	NR	1.60	-	0.083	0.0521	NR	1.50	-	0.00	-	-
34,000 FT.																						
5-15-64	7/697	13:20	1.4	57°	170/15	0	None	1.44	-	0.079	0.0444	NR	1.60	-	0.083	0.0521	NR	1.50	-	0.00	-	-
"	7/698	13:25	1.4	"	"	"	"	1.44	-	0.079	0.0444	NR	1.60	-	0.083	0.0521	NR	1.50	-	0.00	-	-
"	7/699	13:30	1.4	"	"	"	"	1.44	-	0.079	0.0444	NR	1.60	-	0.083	0.0521	NR	1.50	-	0.00	-	-
33,000 FT.																						
5-15-64	7/700	13:35	1.4	"	"	"	"	1.44	-	0.079	0.0444	NR	1.60	-	0.083	0.0521	NR	1.50	-	0.00	-	-
"	7/701	13:40	1.4	"	"	"	"	1.44	-	0.079	0.0444	NR	1.60	-	0.083	0.0521	NR	1.50	-	0.00	-	-

Table XIV.- Summary Of Sonic Boom Data For Various Flights Of Airplane C
For An Altitude Of 49,900 Feet

OPERATING CONDITIONS				WEATHER				SONIC BOOM PRESSURE SIGNATURE DATA														
Date	Flight No.	Time	Mach No.	Surface Temp.	Surface Winds	Cloud Cover	Precipitation	Station 1					Station 3					Station 4				
								ΔP_0	ΔP_1	Δt_0 Pos.	I_0 Pos.	Wave Shape	ΔP_0	ΔP_1	Δt_0 Pos.	I_0 Pos.	Wave Shape	ΔP_0	ΔP_1	Δt_0 Pos.	I_0 Pos.	Wave Shape
2005-4	4/21	9:00	2.0	55°	000/1000	0	None	1.61	1.12	-	-	-	1.62	1.10	0.084	0.1010	N	1.70	1.20	0.085	0.1010	N
2005-4	4/22	9:00	2.0	76°	200/1500	0	SLF	1.62	1.10	-	-	NIR	1.63	-	0.085	0.1010	N	1.62	-	0.085	0.1010	N
2005-4	4/23	9:00	2.0	74°	000/1000	0	None	1.62	-	-	-	N	1.63	-	0.085	0.1010	N	1.63	-	0.085	0.1010	N
2005-4	4/24	9:00	2.0	74°	000/1000	0	-	1.60	-	-	-	N	1.64	-	0.085	0.1010	N	1.64	-	0.085	0.1010	N
2005-4	4/25	9:00	2.0	74°	000/1000	0	-	1.62	-	0.087	0.1010	NIR	1.64	-	0.085	0.1010	N	1.64	-	0.085	0.1010	N
2005-4	4/26	9:00	2.0	74°	000/1000	0	-	1.62	-	0.087	0.1010	NIR	1.64	-	0.085	0.1010	N	1.64	-	0.085	0.1010	N
2005-4	4/27	9:00	2.0	74°	000/1000	0	-	1.62	-	0.087	0.1010	NIR	1.64	-	0.085	0.1010	N	1.64	-	0.085	0.1010	N
2005-4	4/28	9:00	2.0	74°	000/1000	0	-	1.62	-	0.087	0.1010	NIR	1.64	-	0.085	0.1010	N	1.64	-	0.085	0.1010	N
2005-4	4/29	9:00	2.0	74°	000/1000	0	-	1.62	-	0.087	0.1010	NIR	1.64	-	0.085	0.1010	N	1.64	-	0.085	0.1010	N
2005-4	4/30	9:00	2.0	74°	000/1000	0	-	1.62	-	0.087	0.1010	NIR	1.64	-	0.085	0.1010	N	1.64	-	0.085	0.1010	N
2005-4	4/31	9:00	2.0	74°	000/1000	0	-	1.62	-	0.087	0.1010	NIR	1.64	-	0.085	0.1010	N	1.64	-	0.085	0.1010	N

SURFACE TEMPERATURE ----- IN DEGREES FAHRENHEIT

SURFACE WINDS ----- FIRST NUMBER IN COLUMN IS DIRECTION FROM WHICH WIND IS BLOWING
SECOND NUMBER IN COLUMN IS WIND VELOCITY IN KNOTS
PLUS SIGN INDICATES GUSTY
LAST NUMBER FOLLOWING PLUS SIGN IS MAXIMUM VELOCITY

COVER ----- ○ CLEAR
⊙ SCATTERED
⊗ BROKEN
⊕ OVERCAST
X OBSCURATION

PRECIPITATION ----- E SLEET
F FOG
L DRIZZLE
R RAIN
RW RAIN SHOWERS
S SNOW
T THUNDERSTORM
ZL FREEZING DRIZZLE
ZR FREEZING RAIN

BOOM DATA ----- ΔP_o PEAK POSITIVE OUTSIDE GROUND OVERPRESSURE IN LB/SQ FT
 ΔP_i PEAK POSITIVE INSIDE OVERPRESSURE, LB/SQ FT
 Δt_{pos} TIME DURATION OF POSITIVE PHASE OF THE OUTSIDE OVERPRESSURE SIGNATURE, SEC
 $I_{o, pos}$ POSITIVE IMPULSE OF THE OUTSIDE OVERPRESSURE SIGNATURE, LB-SEC/SQ FT

TABLE XVI - THE NUMBER OF DATA RECORDS AT EACH MEASURING STATION FOR
 Approved For Release 2005/05/16 : CIA-RDP71B00622R000100280002-6
 VARIOUS FLIGHT CONDITIONS OF EACH TYPE AIRPLANE

TABLE NUMBER	AIRPLANE TYPE	ALTITUDE, FEET	MACH NUMBER	TOTAL NUMBER OF DATA RECORDS		
				STATION 1	STATION 2	STATION 3
I	A	41,000	2.0	3	3	3
↓		38,000	1.5	8	9	8
↓		37,600	↓	1	1	1
↓		37,500	↓	1	1	1
↓		37,000	↓	6	4	5
II		36,000	↓	10	9	10
↓		35,000	2.0	1	1	1
↓		↓	1.7	1	1	1
↓		↓	1.5	26	26	25
↓		34,000	1.8	1	1	1
↓		33,000	1.7	1	1	1
III		↓	1.5	2	2	2
↓		32,000	1.8	3	3	3
IV		↓	1.5	103	101	106
↓		31,000	↓	17	17	17
V		30,000	1.8	2	2	1
↓		↓	1.7	76	78	74
VI		↓	1.5	68	70	69
↓		29,000	1.8	1	1	1
↓		↓	1.7	27	26	25
↓		↓	1.5	29	29	26
↓		↓	1.55	1	1	1
VII		28,000	1.7	34	33	34
↓		↓	1.5	168	169	155
VIII		27,000	1.7	5	5	5
↓		↓	1.5	8	8	8
↓		↓	1.3	5	4	4
IX		26,000	1.5	2	2	2
↓		24,000	↓	11	11	11
↓		↓	1.4	8	8	7
X		↓	1.3	1	1	1
↓		23,000	1.6	1	1	1
↓		↓	1.5	2	2	1
↓		↓	1.4	2	4	4
↓		↓	1.3	11	13	13
↓		21,000	1.5	3	3	3
↓	B	↓	1.4	3	3	3
XI		46,000	1.5	21	21	21
↓		↓	1.4	7	8	8
XII		44,000	1.5	57	58	58
↓		42,000	↓	3	3	3
XIII		↓	1.4	4	4	3
↓		40,000	↓	3	3	2
↓		38,000	↓	13	13	13
↓		34,000	↓	3	3	3
↓		33,000	↓	2	2	2
XIV	C	49,900	2.0	8	8	8

TABLE XVII.- SUMMARY OF MEASURED AND CALCULATED OUTSIDE SONIC BOOM OVERPRESSURES AND IMPULSES FOR THREE MEASURING STATIONS
(DATA ARE FOR AIRPLANE "A" AND FOR THOSE CONDITIONS WHERE A LARGE NUMBER OF DATA POINTS EXIST)

AIRPLANE TYPE	ALTITUDE FEET (MSL)	MACH NO.	STATION 1						STATION 3						STATION 4					
			OUTSIDE OVERPRESSURE ΔP_o , LB/SG FT			OUTSIDE IMPULSE POSITIVE $I_{o \text{ pos}}$, LB-SEC/SG FT			OUTSIDE OVERPRESSURE ΔP_o , LB/SG FT			OUTSIDE IMPULSE POSITIVE $I_{o \text{ pos}}$, LB-SEC/SG FT			OUTSIDE OVERPRESSURE ΔP_o , LB/SG FT			OUTSIDE IMPULSE POSITIVE $I_{o \text{ pos}}$, LB-SEC/SG FT		
			CALC. NOMINAL	MEDIAN @ 50%	MEDIAN @ 1%	CALC. NOMINAL	MEDIAN @ 50%	MEDIAN @ 1%	CALC. NOMINAL	MEDIAN @ 50%	MEDIAN @ 1%	CALC. NOMINAL	MEDIAN @ 50%	MEDIAN @ 1%	CALC. NOMINAL	MEDIAN @ 50%	MEDIAN @ 1%	CALC. NOMINAL	MEDIAN @ 50%	MEDIAN @ 1%
A	28,000	1.5	1.59	1.12	2.02	.0372	.0245	.0345	1.23	1.24	2.72	.0311	.0255	.0385	0.88	0.80	2.28	.0229	.0165	.0240
A	30,000	1.5	1.45	1.04	1.78	.0347	.0240	.0350	1.15	1.20	—	.0300	.0250	.0380	0.83	0.80	2.28	.0219	.0170	.0310
A	32,000	1.5	1.31	1.08	1.87	.0322	.0260	.0375	1.06	1.04	2.00	.0280	.0235	.0345	0.78	0.74	1.44	.0208	.0175	.0260
A	30,000	1.7	1.53	0.90	2.10	.0357	.0235	.0310	1.22	0.94	2.36	.0390	.0245	.0345	0.87	0.82	1.57	.0241	.0175	.0265

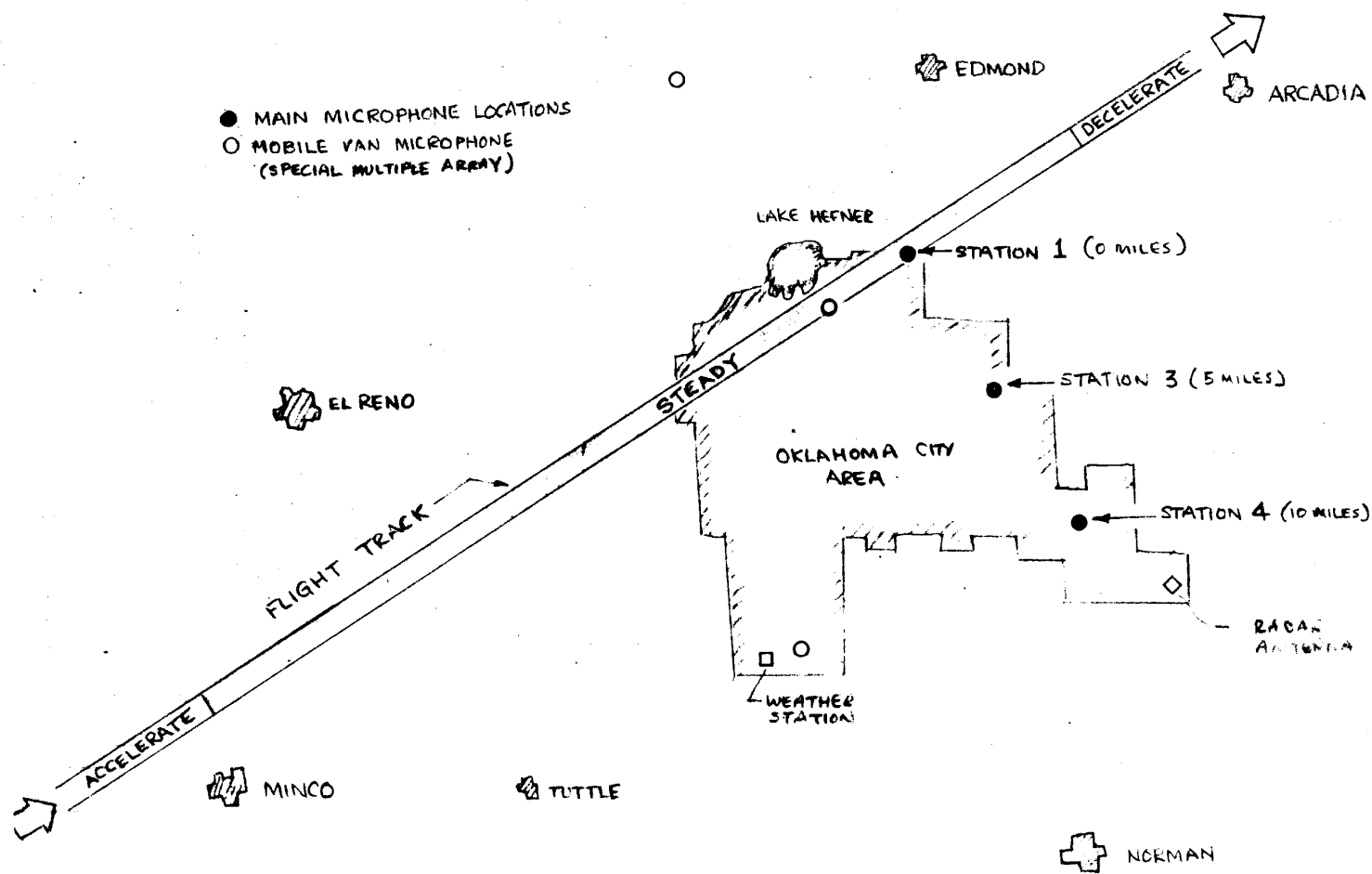


Figure 1. - Planview sketch of test area showing flight track, measuring stations and facilities.

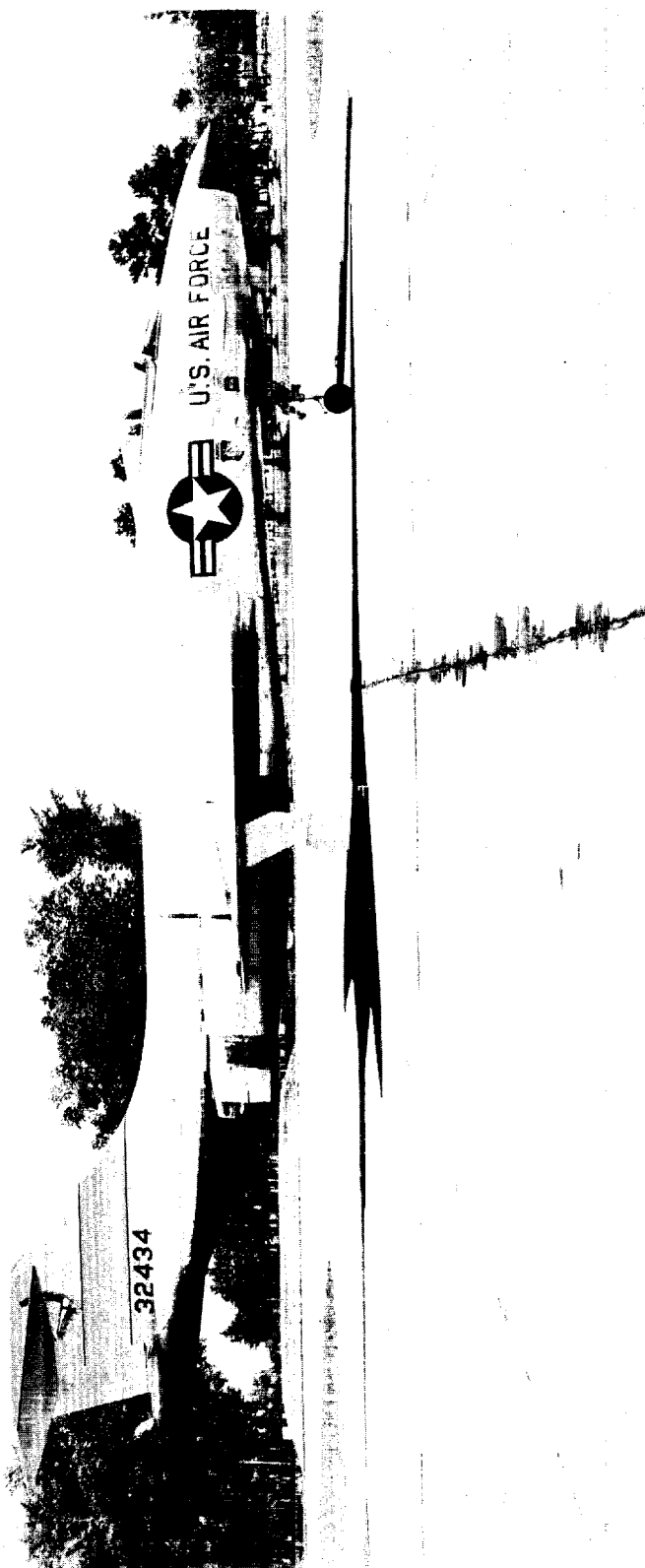
Approved For Release 2005/05/16 : CIA-RDP71B00822R000100280002-6



(a) Airplane 1.

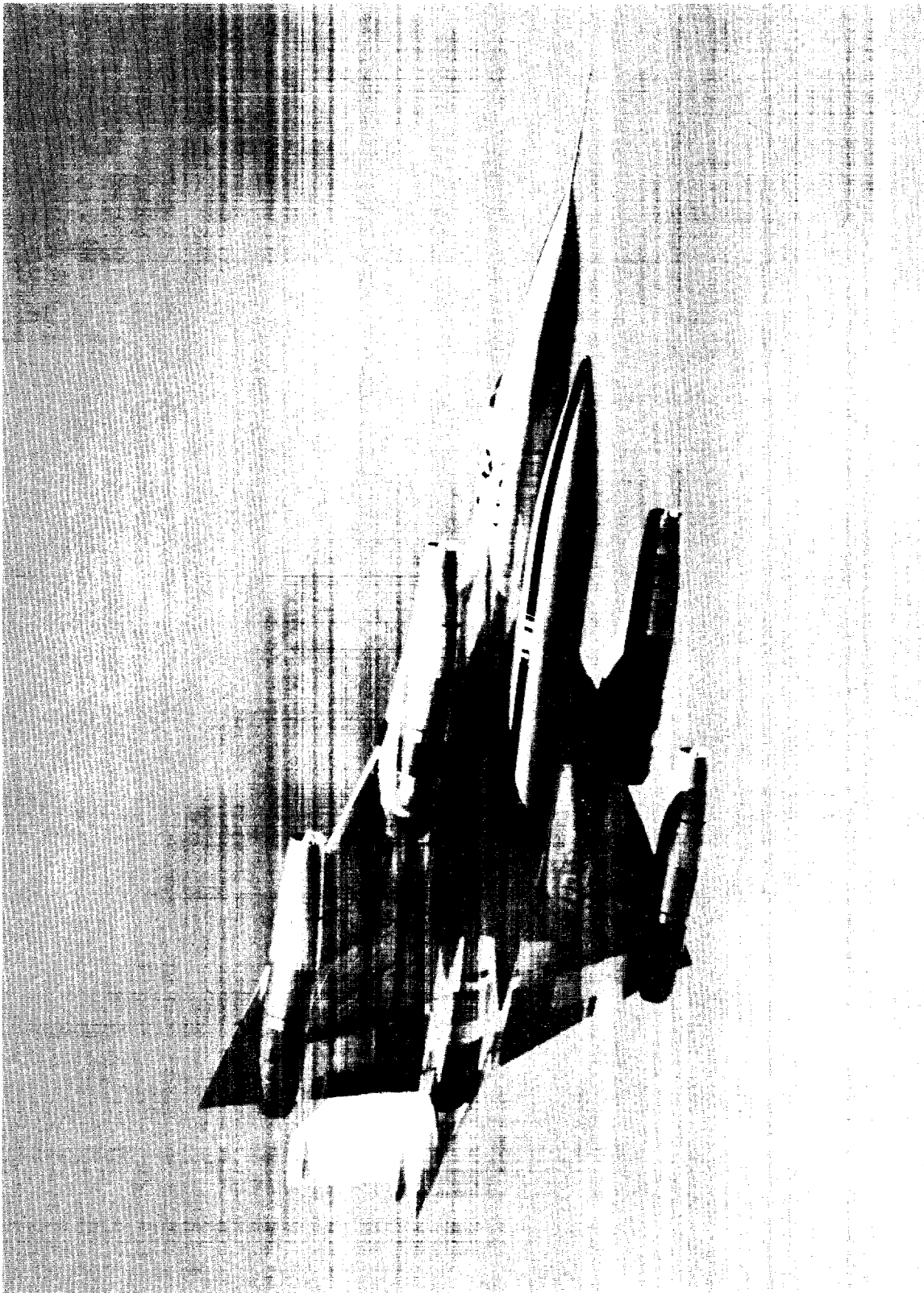
Figure 2. - Photographs of airplanes of the types used in the Cuban Missile Crisis.

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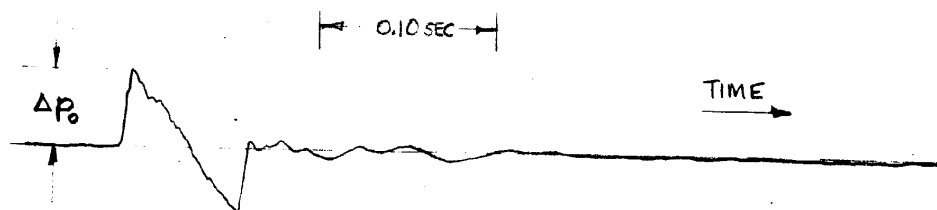


(B) Airplane B.

Figure 2 - Continued.



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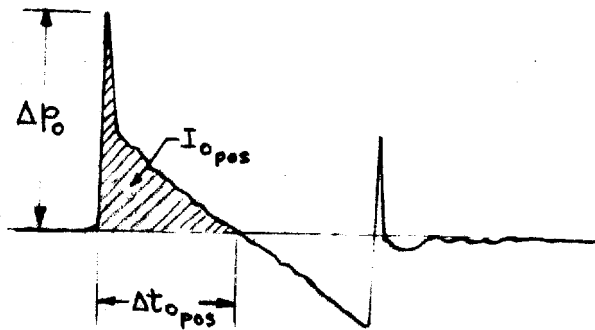
(a) Outside microphone.



(b) Inside microphone.

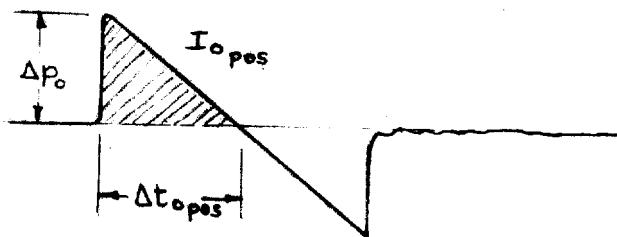
Figure 2. - Sample sonic boom pressure time histories for both inside and outside microphone locations. (Data are for airplane A at station 1)

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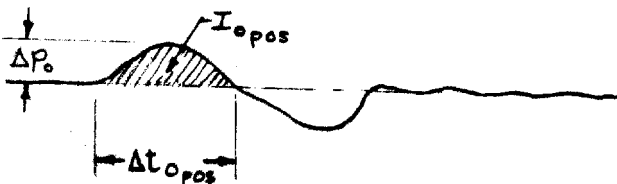
PEAKED WAVE WITH VERY SHORT
RISE TIME ASSOCIATED WITH
INITIAL PEAK.

(a) Type P.



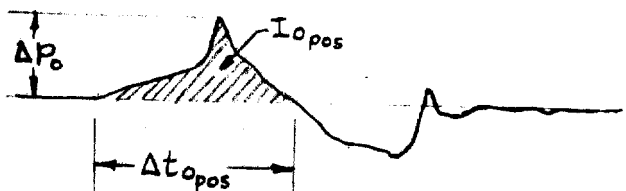
APPROXIMATELY N-WAVE IN SHAPE

(b) Type N.



ROUNDED-OFF WAVE HAVING
SINE-WAVE TYPE APPEARANCE.

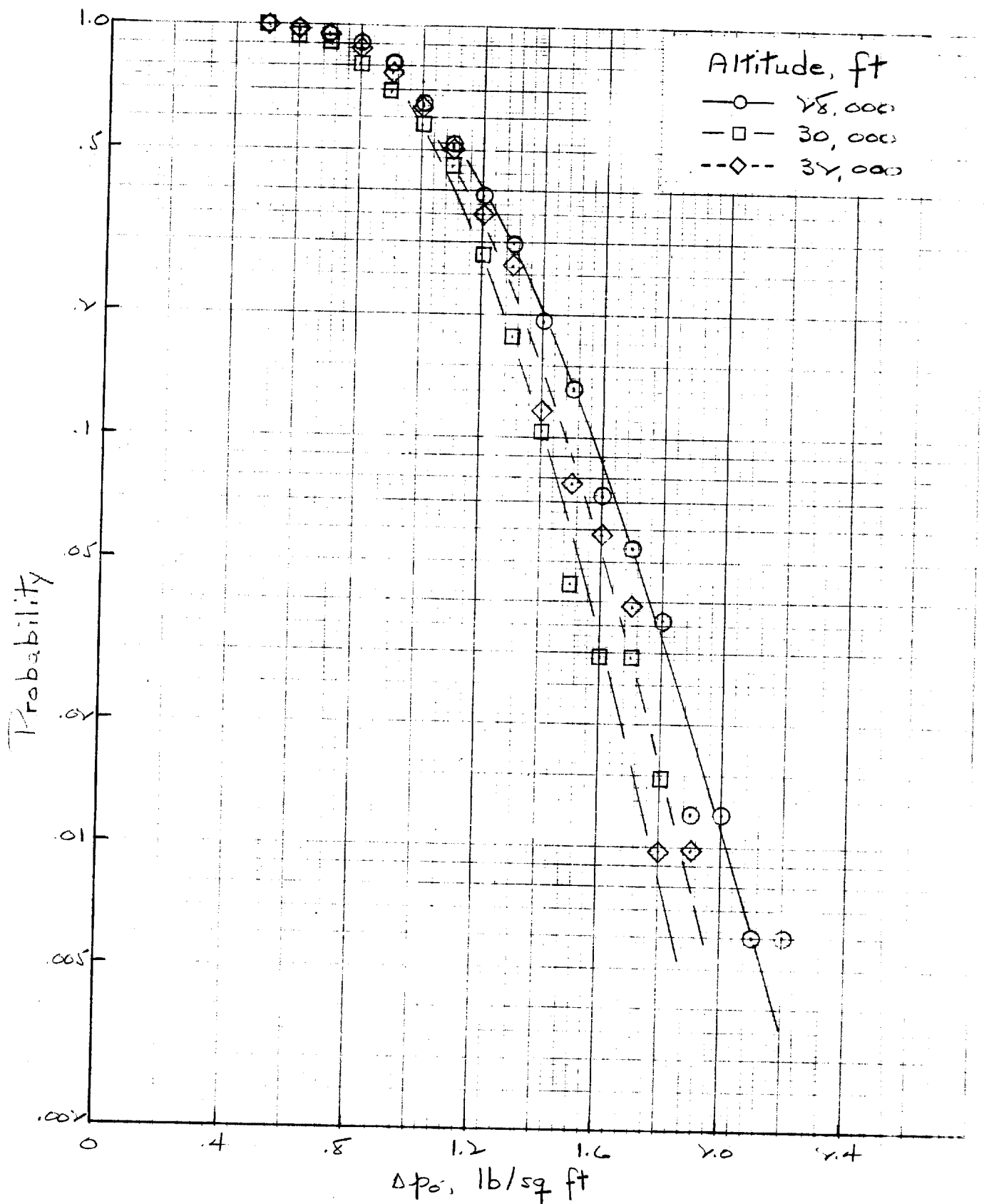
(c) Type R.



PEAKED WAVE WITH LONG RISE TIME

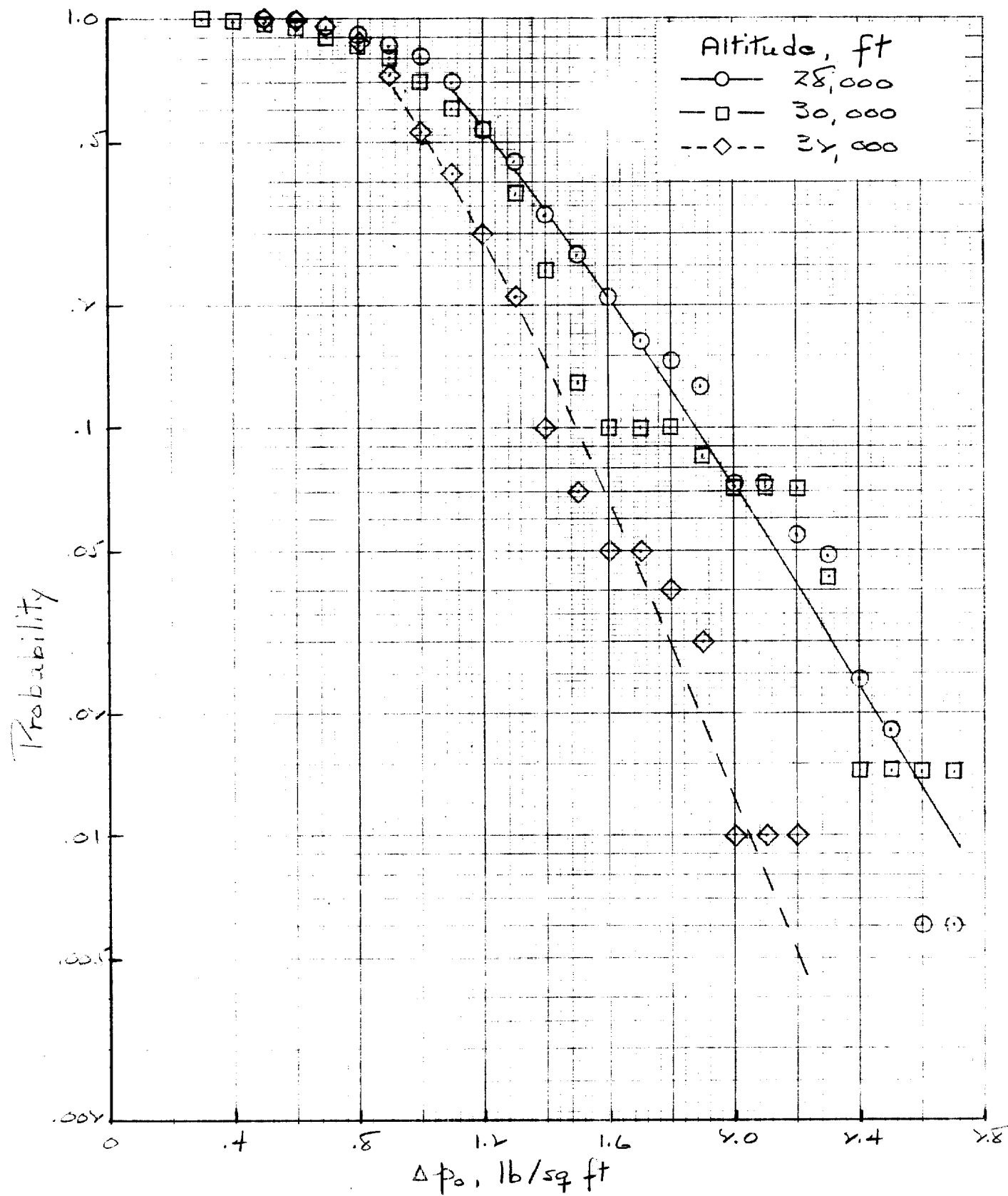
(d) Type C.

Figure 4. - Schematic diagrams showing some categories of waveforms
measured at ground level during the tests.

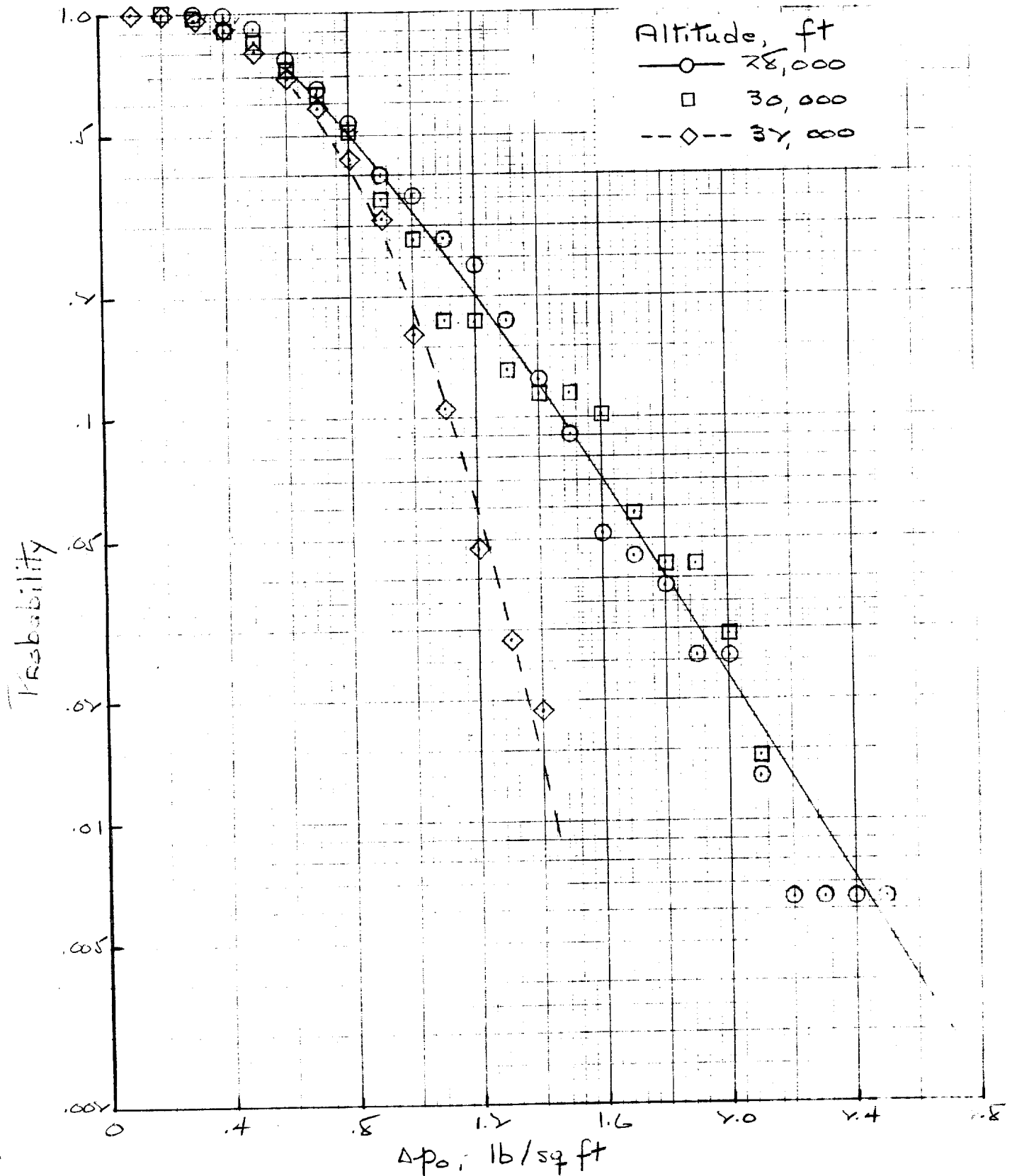


(a). Measuring station 1.

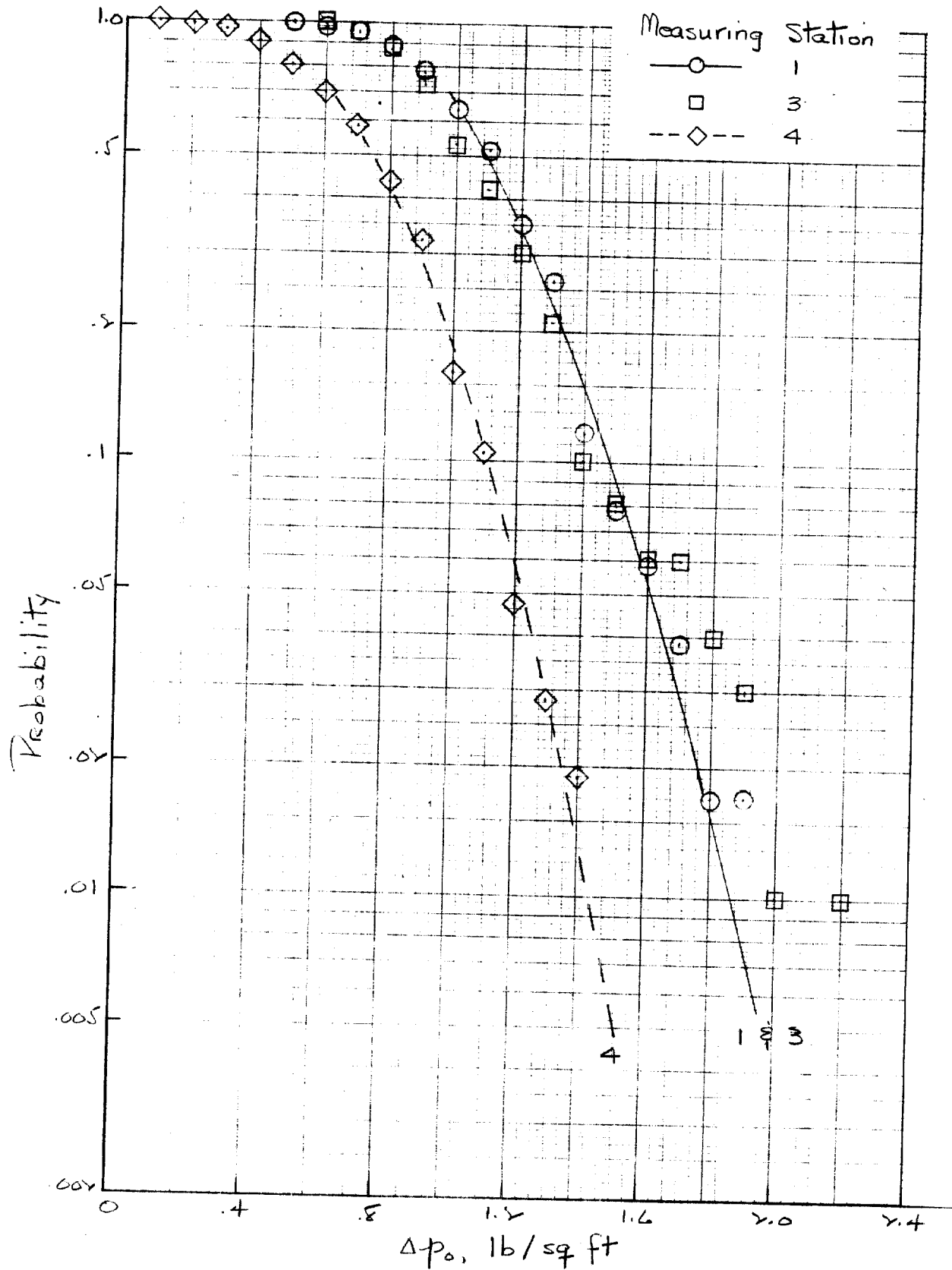
Figure 5. - Probability of equaling or exceeding a given sonic boom ground overpressure.
 Approved For Release 2005/05/16 : CIA-RDP71B00822R000100280002-6
 Data for airplane A at Mach No. 1.5.



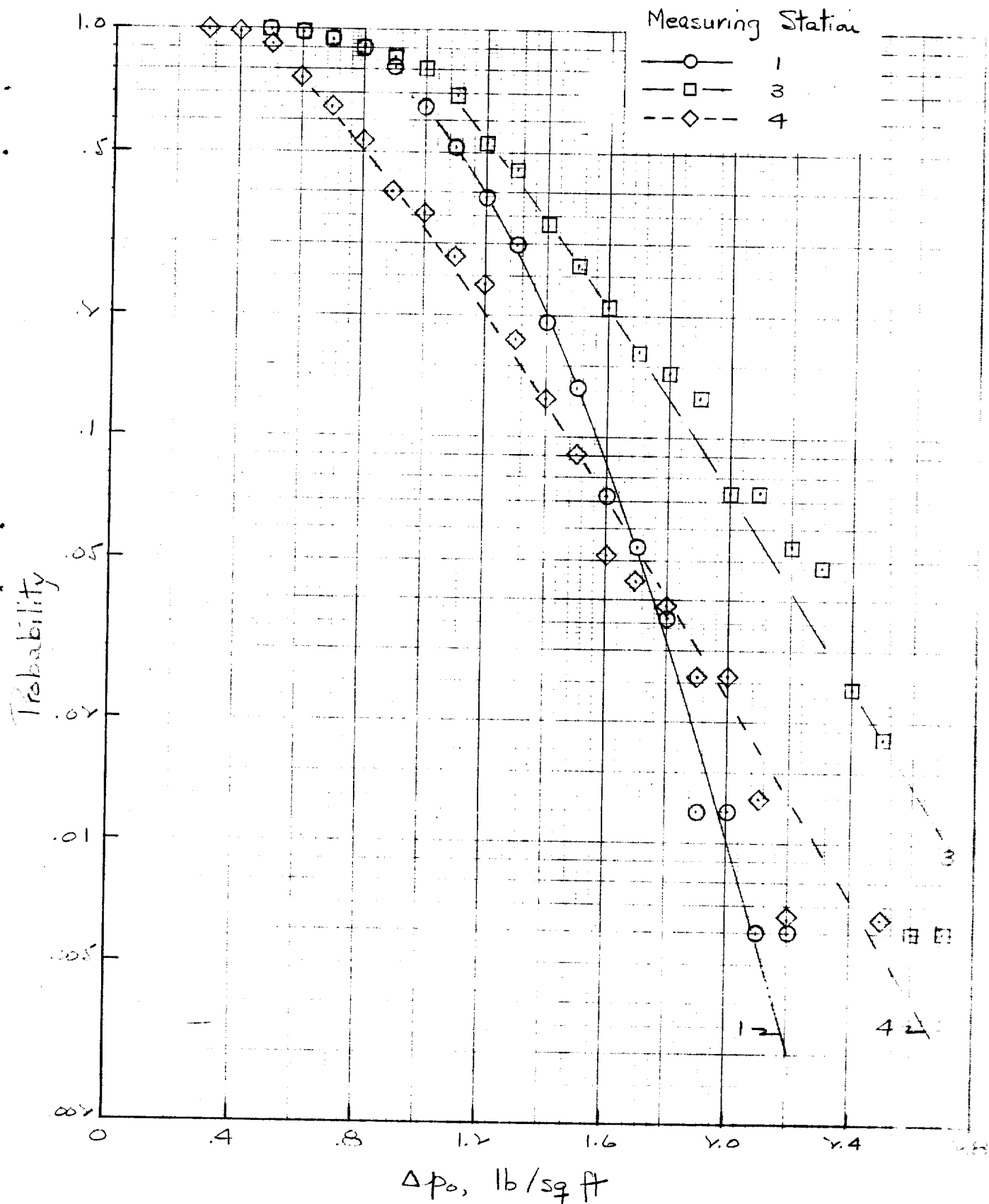
(b) Measuring station 3.



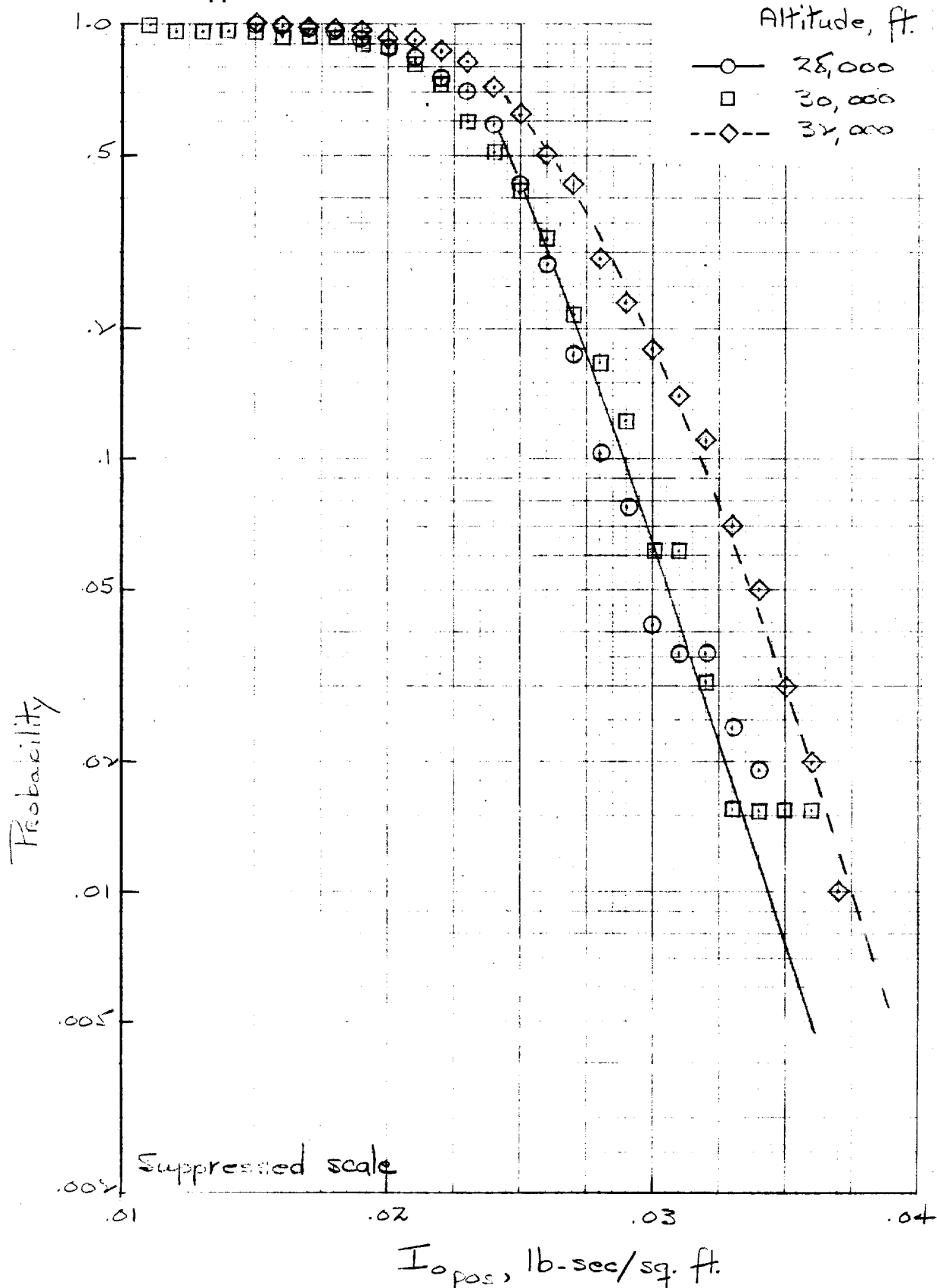
(c) Measuring station 4.



(a) Airplane altitude 32,000 feet.

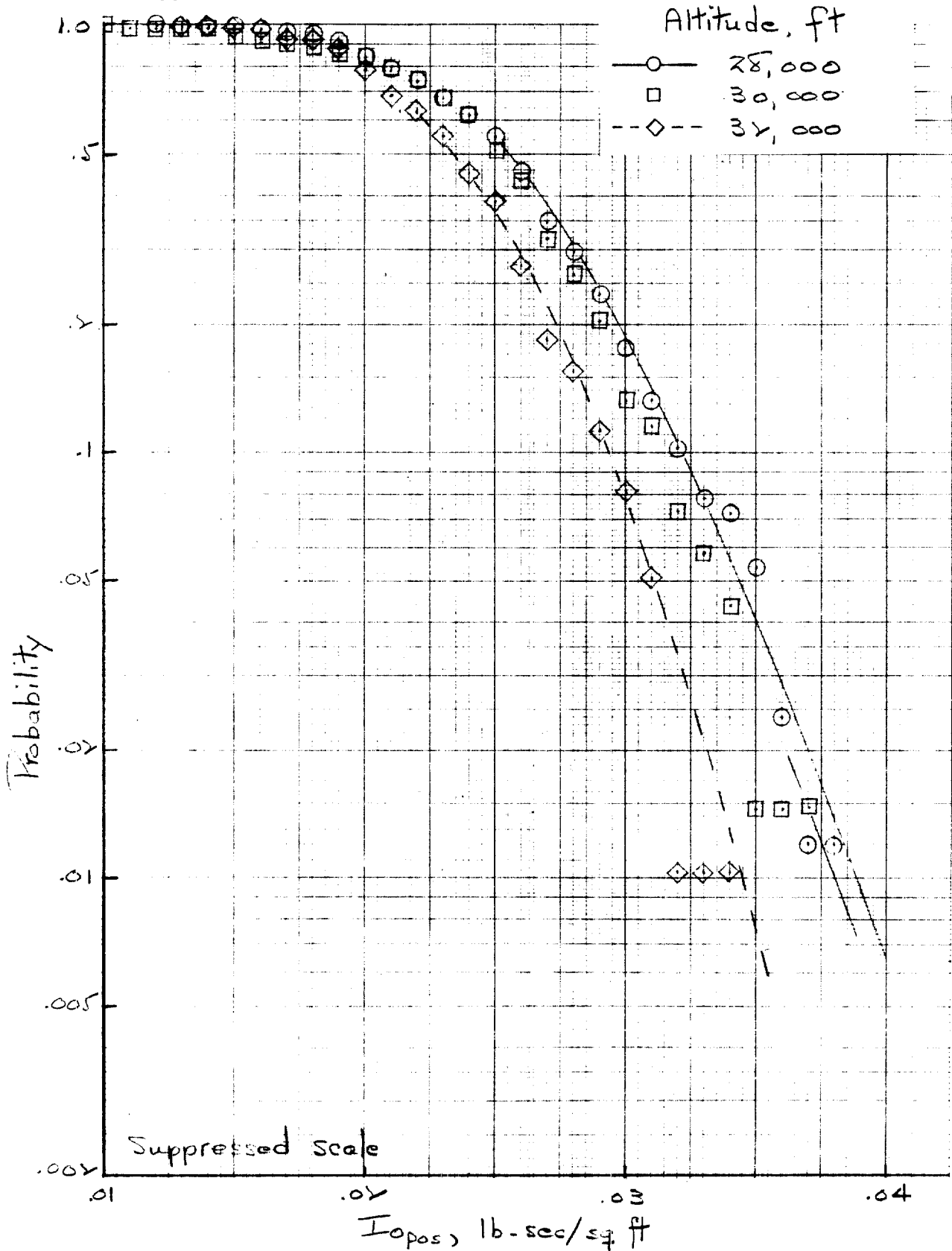


(b) Airplane altitude 28,000 feet.

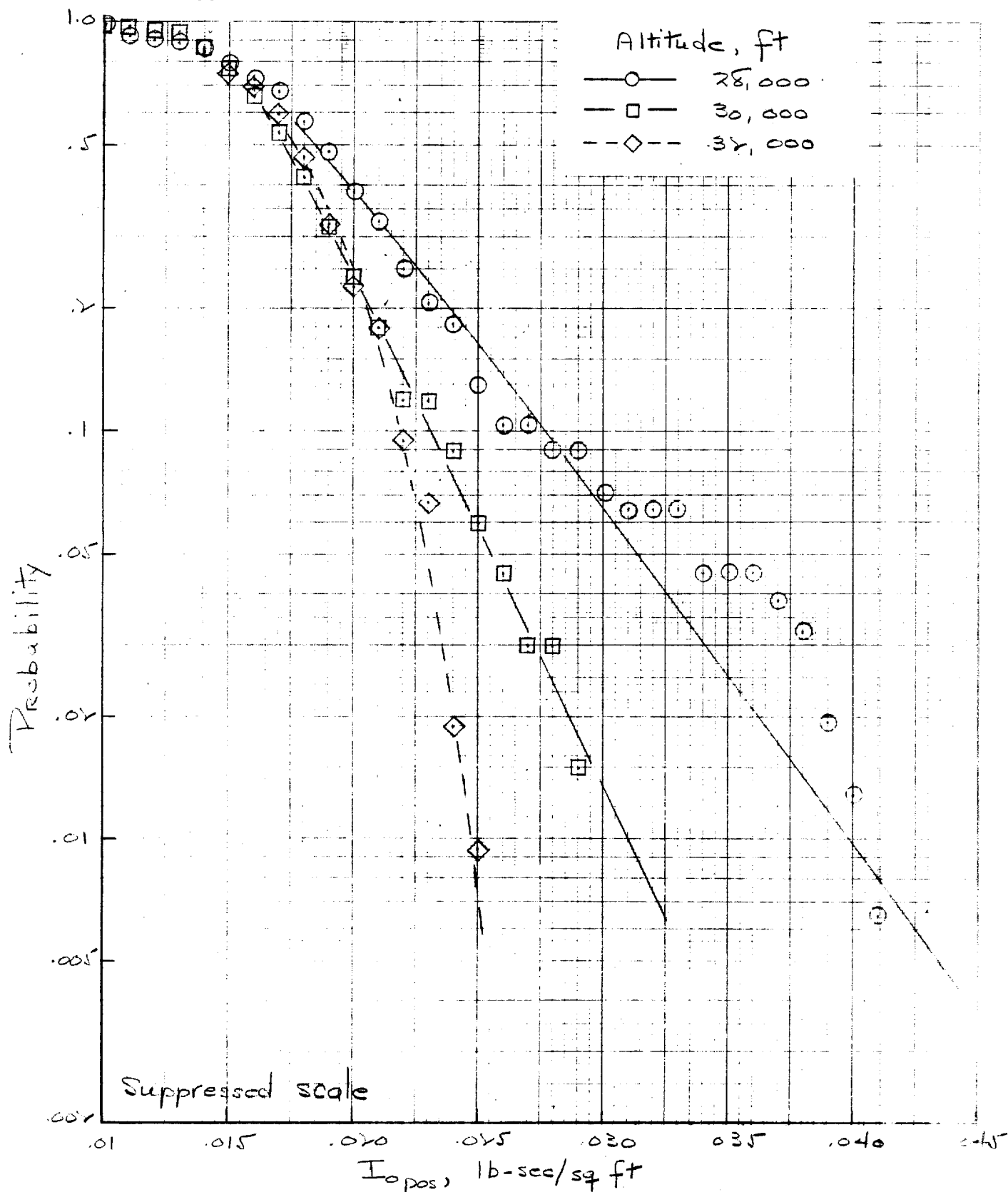


(a) Measuring station 1.

Figure 7. - Probability of equaling or exceeding a given positive impulse.



(b) Measuring station 3.



(c) Measuring station 4.

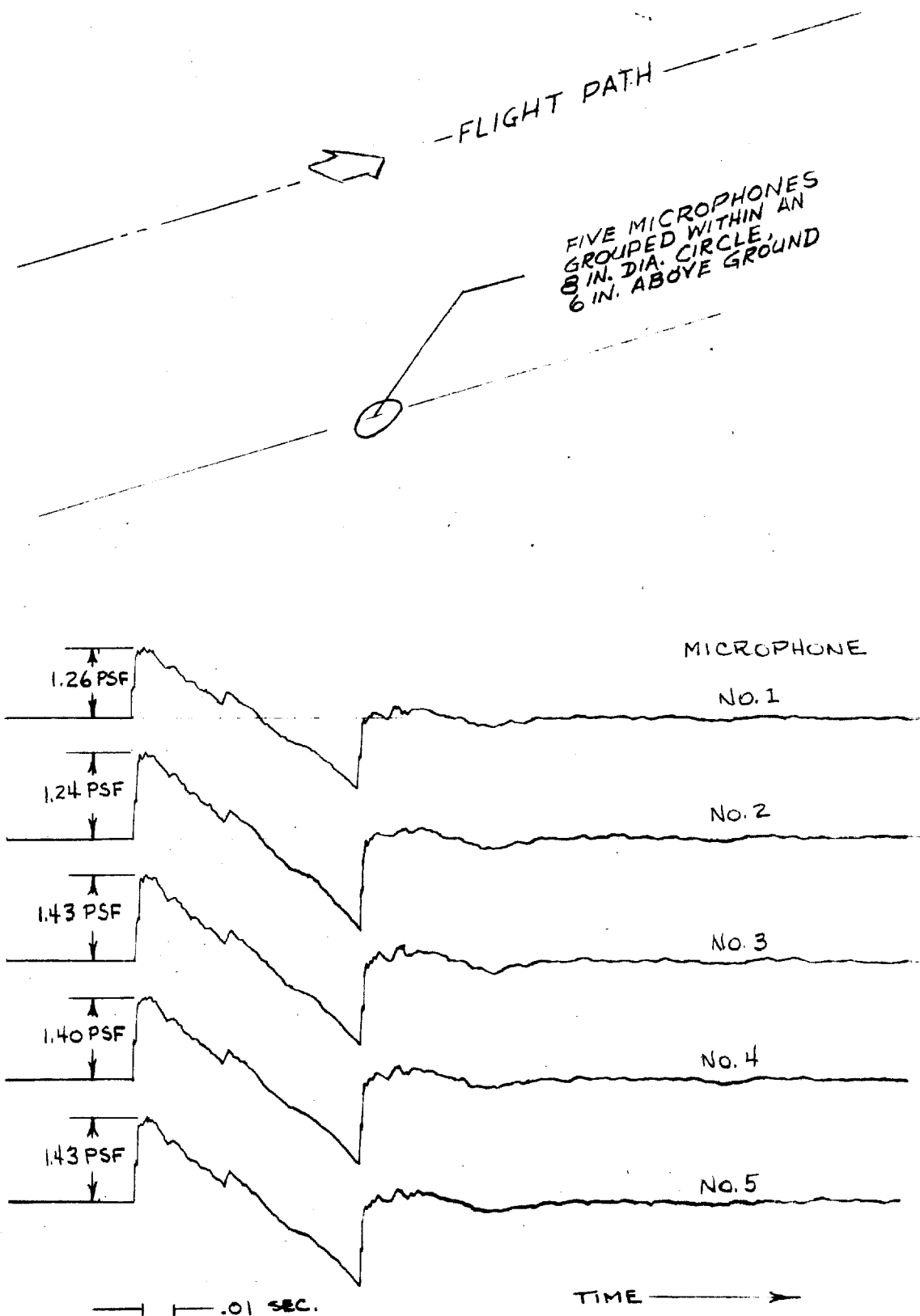
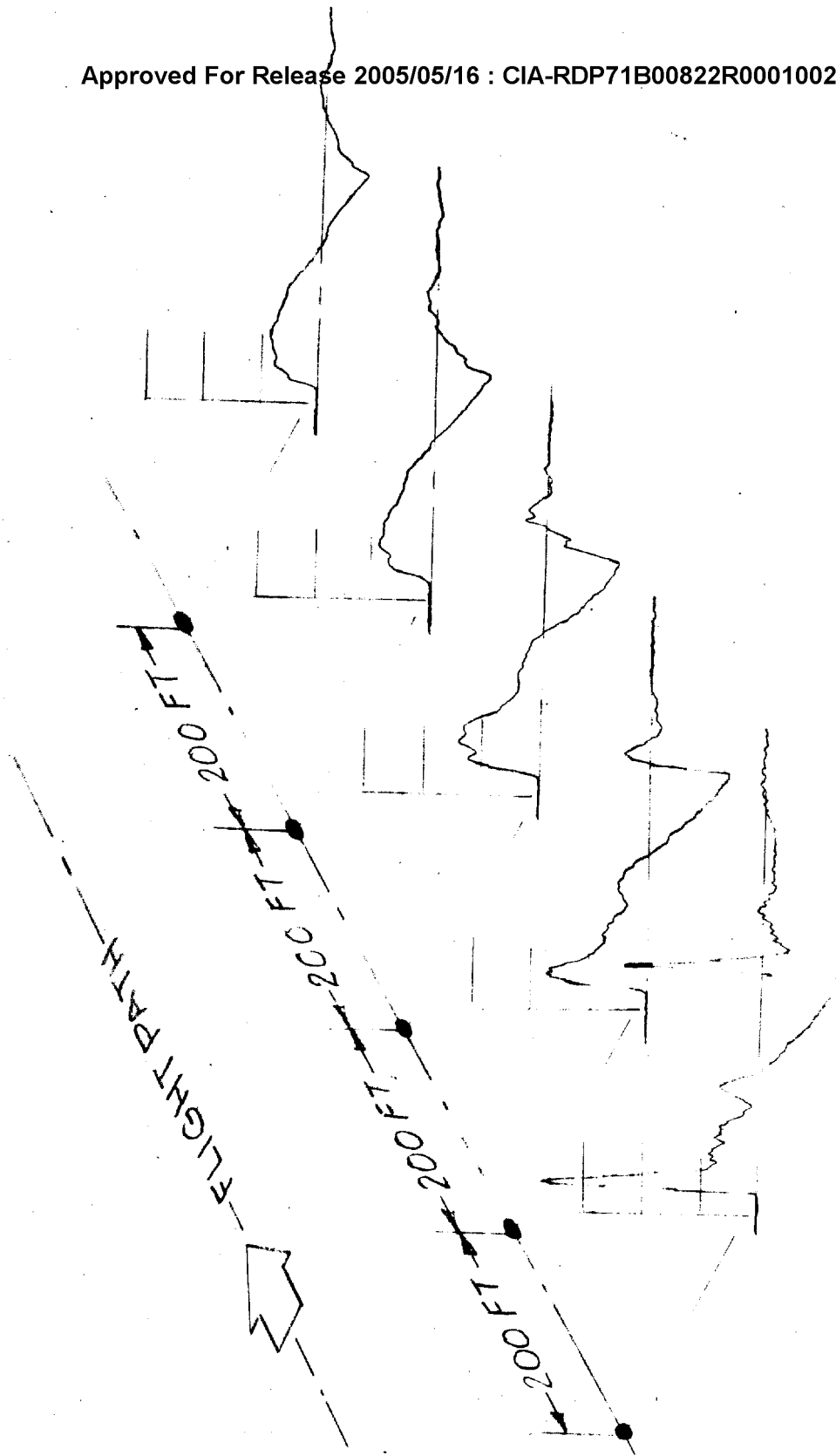
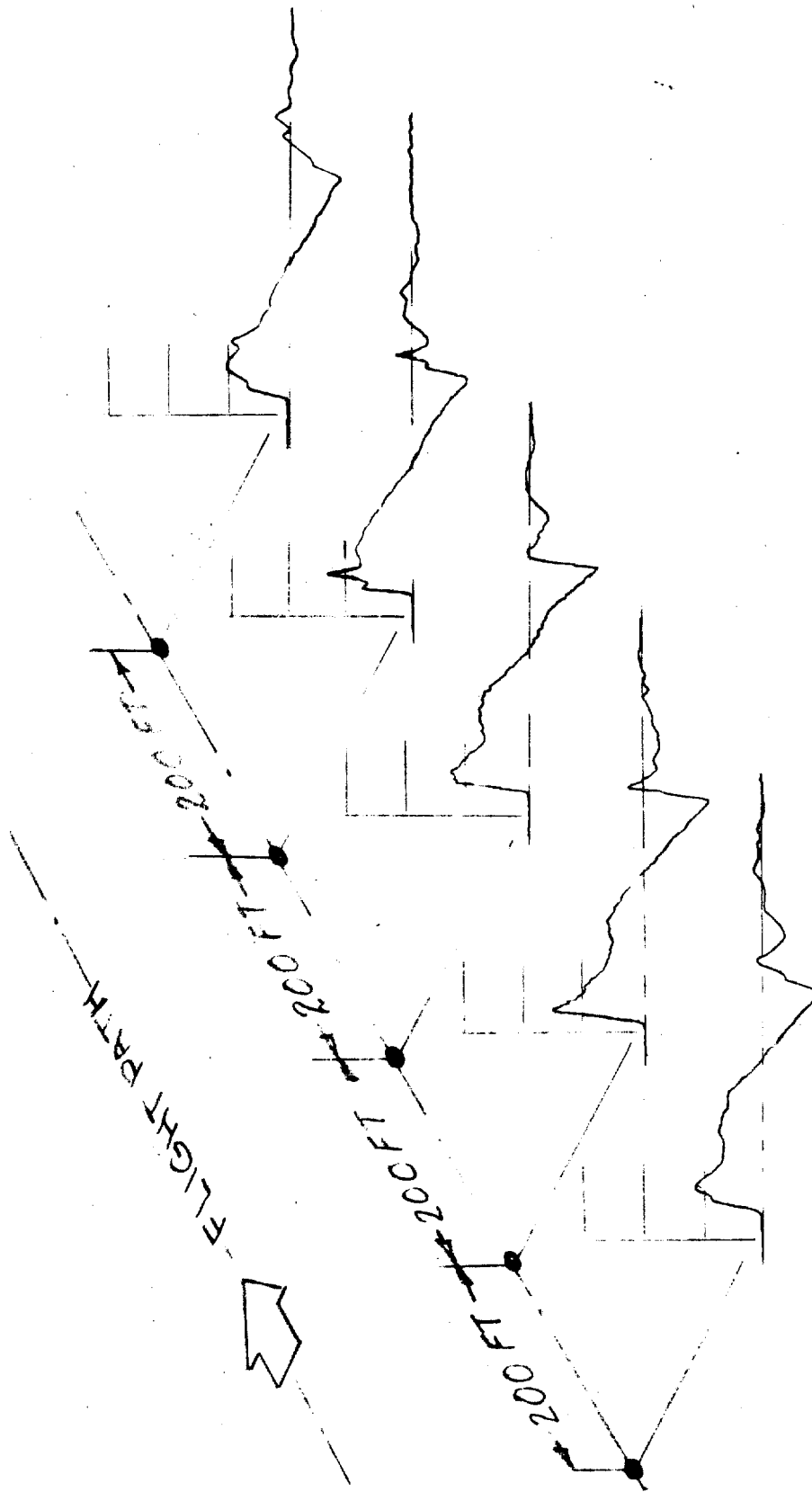


Figure 8. - Sonic boom pressure signatures for airplane A at an altitude of 28,000 feet and a Mach number of 1.5 from five microphones grouped within 8 inches of the ground.



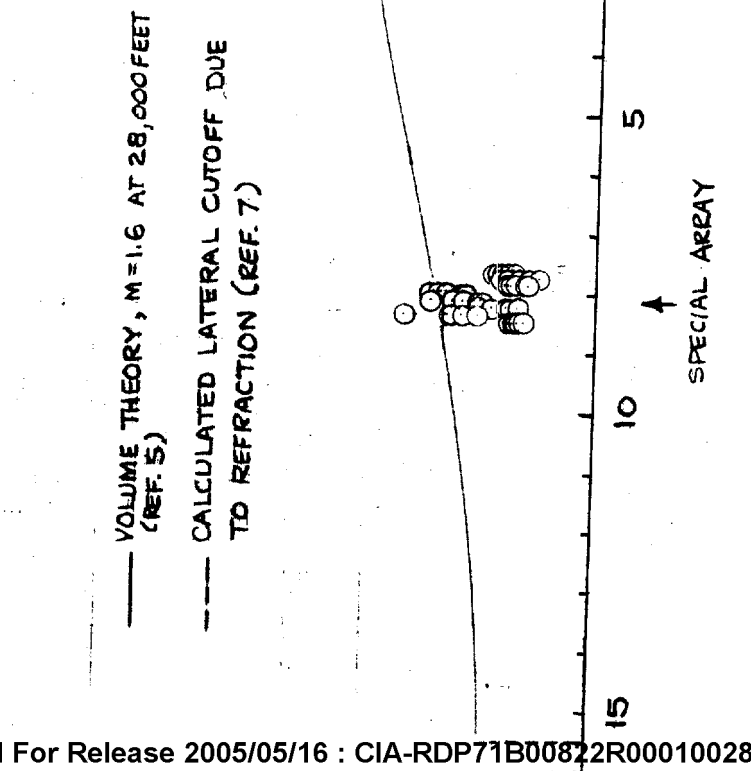
(a). Time of flight 0730 hours.

Figure 1. Measured sonic boom pressure signatures at several points along the ground track of airplane A in steady-level flight at Mach number 1.7 and an altitude of 28,000 feet at different times of day.



(b) Time of flight 0030 hours.

Figure 2 - Continued.



LATERAL DISTANCE FROM TRACK, MILES

Figure 10. - Measured ground overpressures at several measuring stations at different distances from the ground track. Data are for eight flights of airplane A on April 6, 1964 for an altitude of 28,000 feet at Mach numbers of 1.5 and 1.7.

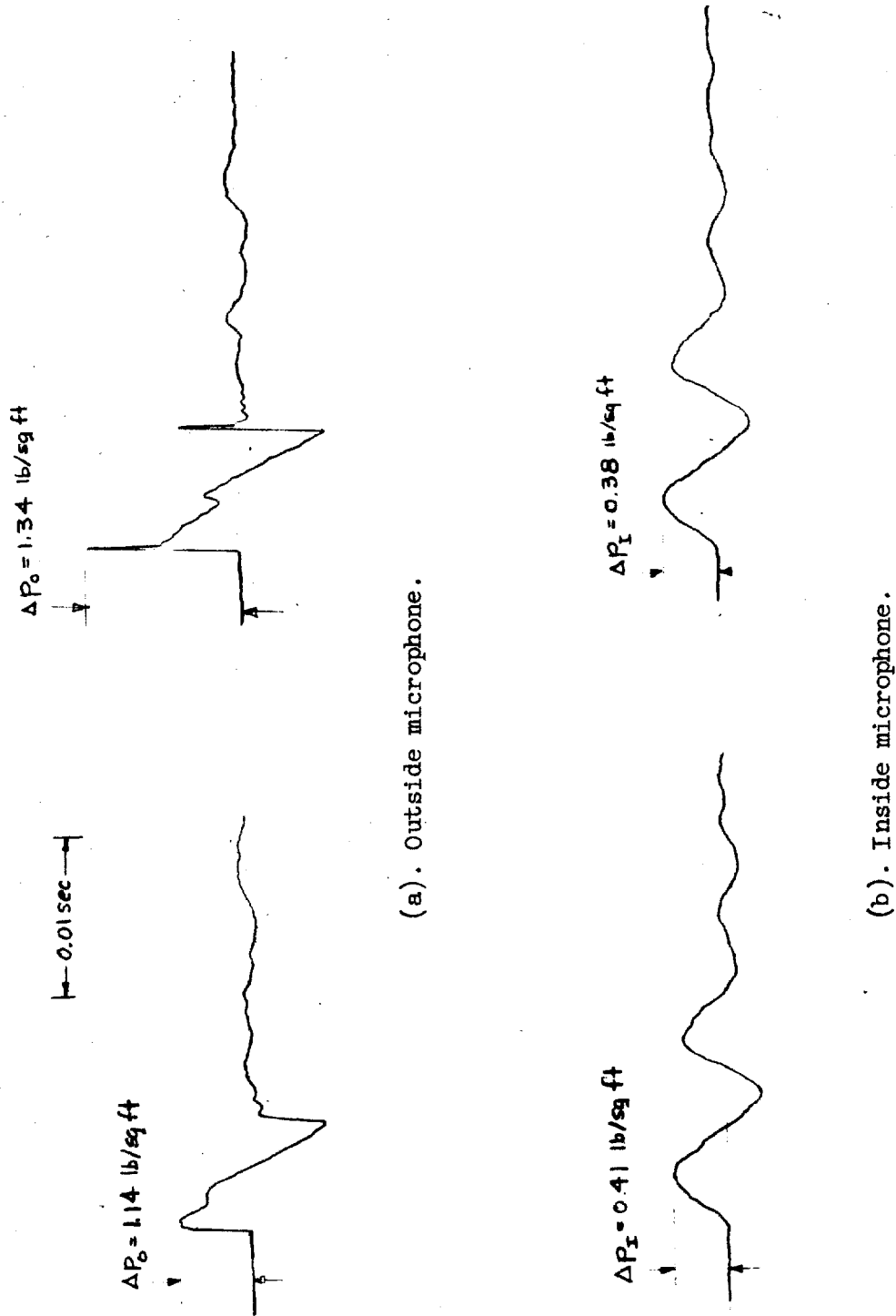


Figure 11. - Measured outside and inside pressure traces at station 1 for two different flights of airplane A.

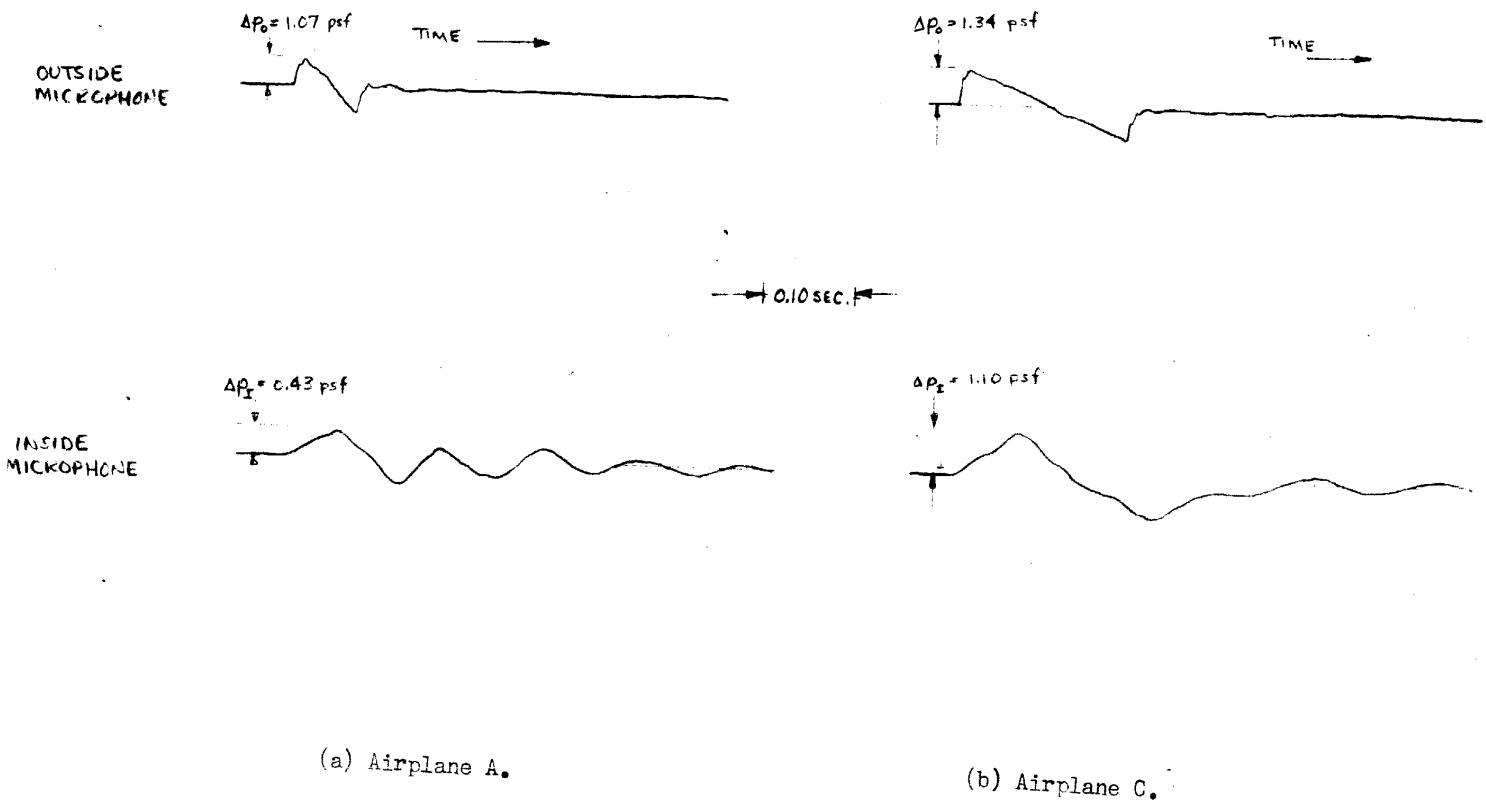


Figure 12. - Measured outside and inside pressure traces at station 1 for airplanes A and C.

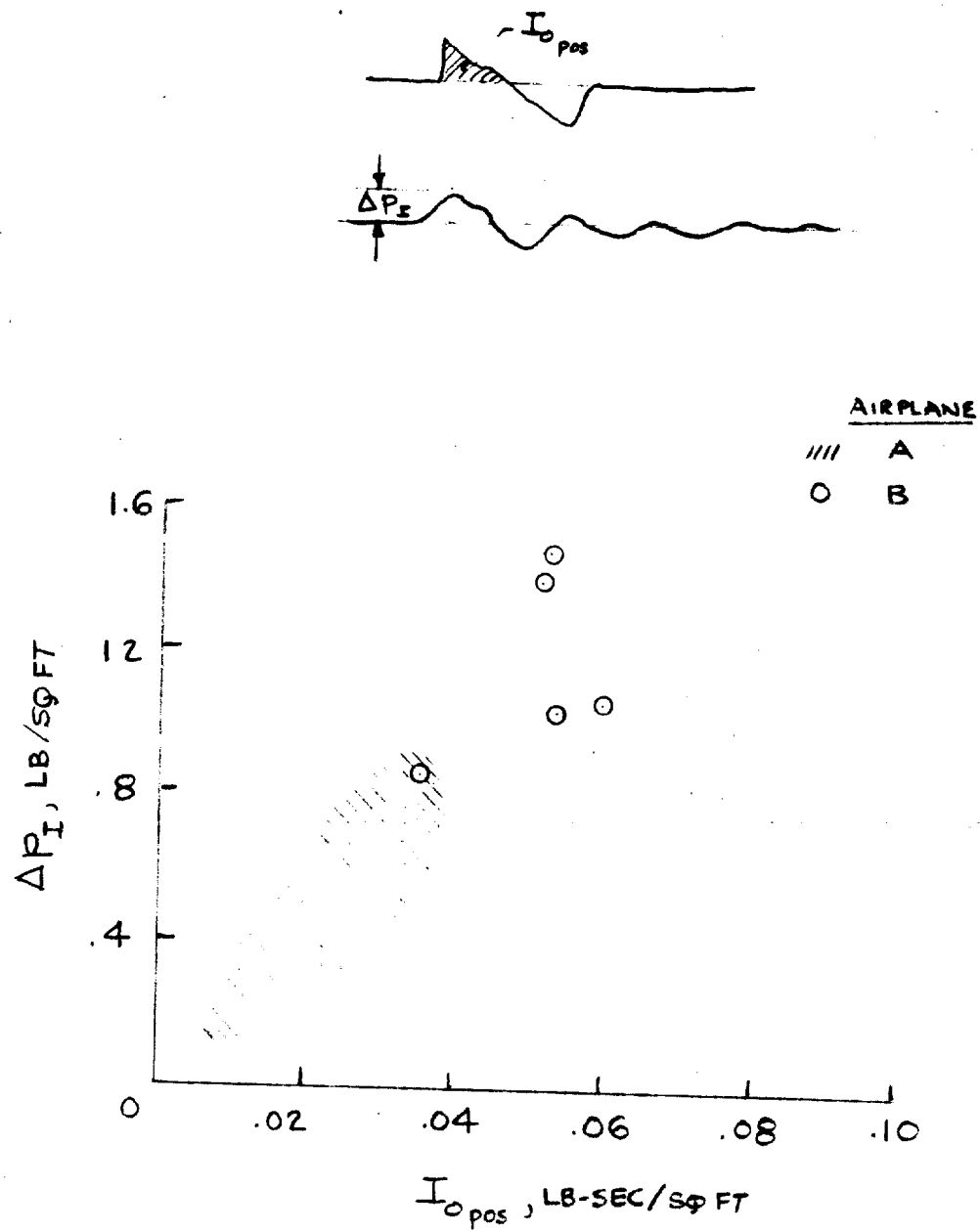


Figure 13. - Measured inside peak overpressure as a function of outside positive impulse as measured at station 1 for airplanes A and B.